

REINHOLD ENVIRONMENTAL Ltd.



**2017 APC & Wastewater Round Table
& Expo Presentation**

July 17 & 18, 2017 in Charlotte, NC / Hosted by Duke Energy

All presentations posted on this website are copyrighted by Reinhold Environmental, Ltd (RE). Any unauthorized downloading, attempts to modify or to incorporate into other presentations, link to other websites, or obtain copies for any other uses than the training of attendees to RE's Conferences is expressly prohibited, unless approved in writing by RE or the original presenter. RE does not assume any liability for the accuracy or contents of any materials contained in this library which were presented and/or created by persons who were not employees of RE.

What's the Best Approach for Controlling Forced Oxidation Air Rates?

Presented at the Reinhold APC & Wastewater
Roundtable, Charlotte NC

Gary Blythe, AECOM

July 18, 2017

AECOM

Why Control Forced Oxidation Air Rates?

- Historically not required on LSFO FGD systems
 - Large coal units typically base loaded
 - Higher than needed air rates at low load ensure low liquid-phase sulfite, high gypsum purity
 - Minor auxiliary power savings generally not important

Why Control Forced Oxidation Air Rates (cont'd)?

- More drivers to control ox air rates today:
 - More coal units cycling and operating at low load
 - Under-deposit corrosion issues in alloy absorbers
 - Wet FGD used as a mercury control device
 - ELGs likely to require control of Hg, As, Se, NO_3^- in FGD wastewater discharges
 - Concentrations of all of these species can be impacted by sulfite oxidation rate in FGD
 - Better net heat rate makes plant more competitive
- All of these drivers lead to a need to control ox air rates as sulfur capture rate varies

How to Best Control Forced Oxidation Air Rates?

1. No control; deal with the consequences
2. Control ox air rates based on slurry ORP
3. Use empirical, feed-forward control strategy
4. Measure liquid-phase sulfite concentrations, vary ox air rate to control to set point

Option 1. Don't Turn Down Ox Air Rates at Low Load and/or Low Inlet SO₂

- Dissolved sulfite concentration below detection limits
- High ORP (>300 mV) at low load/inlet SO₂
- Hg in slurry transfers back to liquor phase, can re-emit or:
 - High PAC injection rates required upstream of FGD to control Hg in flue gas below MATS limit
 - High addition rates of re-emission additive to lower ORP, control re-emission
- Selenite in liquor oxidizes to selenate (w/o additive)
- Dissolved manganese oxidizes, precipitates on wetted surfaces; possible under-deposit corrosion (w/o additive)

Dealing with Over-oxidizing Conditions When Forced Ox Air Rates are too High

–Hg control:

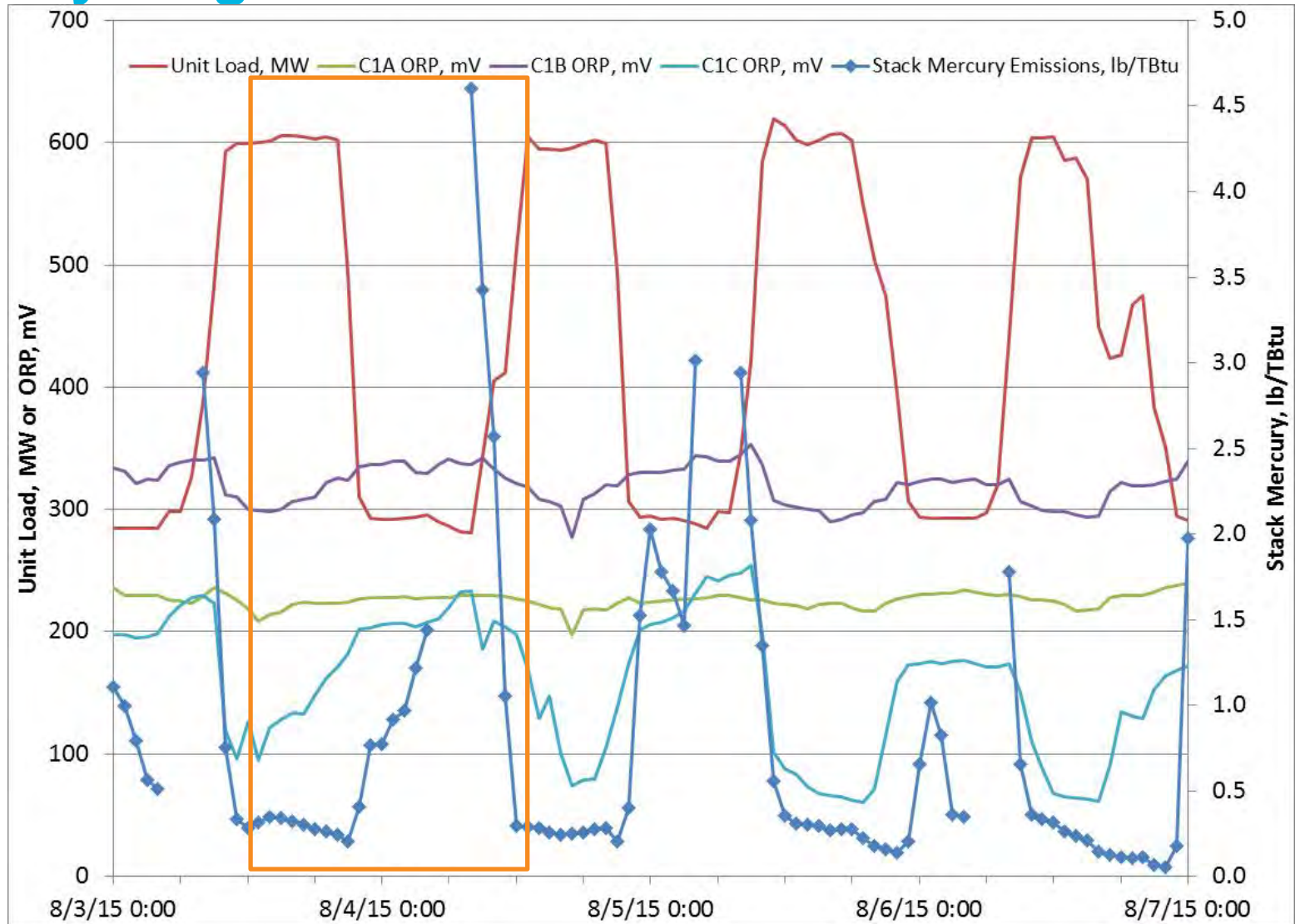
- Inject PAC upstream to control Hg below MATS limit at FGD inlet, and/or
- Use re-emission additives to control sulfite oxidation rate/ORP, transfer Hg to FGD slurry solids

–Design wastewater treatment to handle high dissolved Hg, SeO_4^- , NO_3^-

–Apply measures to prevent under-deposit corrosion

- Potential Adjustment Protection (PAP)
- Wallpaper with higher alloy
- Apply protective coatings
- Use re-emission additive to control sulfite oxidation rate

Example Data for Forced Ox Air at Maximum Rate with Cycling Load



Adjusting Forced Ox Air Rates to Respond to Unit Load, Inlet SO₂ Changes (Options 2-4)

- Turndown of air rates is limited on many FGD systems (a common issue)
- Range of turndown depends on blower/compressor type, ox air system design, type of air sparger in reaction tank

Modifying Forced Ox Air Systems to Increase Turndown

- Replace manual valves with remotely operated valves
- Modify piping so one blower can supply air to two FGD systems
- Possibly use VFD on blower motor
- Add or increase size of blow-off valves/silencers
- Take some fixed-sparger headers out of service



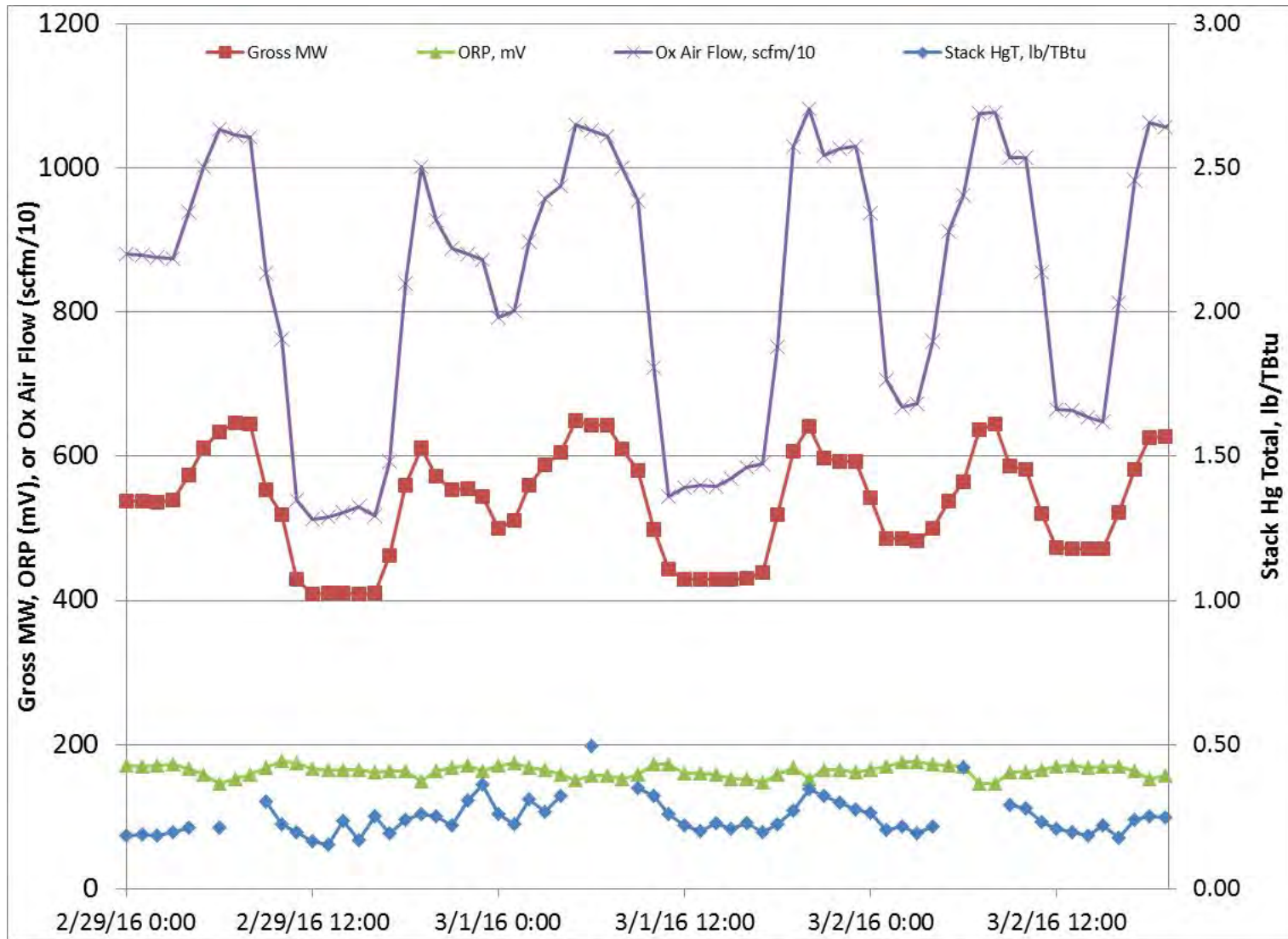
Option 2. Adjust Forced Ox Air Rates to Control ORP

- Automating control may be covered by MHI patent
- Manual adjustment approach requires considerable operator attention
 - Operators unsure how big an adjustment to make on air rates
 - Air flow rate instruments often inaccurate or inoperable, makes it difficult for operators to gauge “where they are”
- How reliable is ORP measurement?
 - Probes require as much diligence to maintain as pH
 - ORP measurements impacted by other redox reactions in wet FGD slurry

Option 3. Empirical Correlation to Control Forced Ox Air Rate

- Automate forced ox air rates to adjust for unit load, FGD inlet SO₂ concentration
- Empirical control algorithm programmed into DCS
 - Upgraded air flow instrumentation may be needed
 - Works best with a reliable inlet SO₂ monitor
 - Need to account for higher O₂ in flue gas at low load & for number of recycle pumps running
- No slurry probes or monitors needed, but:
 - Fine tuning may be needed to control sulfite oxidation rates over full range of unit load, coal S
 - Provide operator over-ride capability

Example Data with Feed Forward Forced Ox Air Control



Option 4. Use Sulfite Monitor for Feedback Control of Forced Ox Air Rate

- Proprietary instrument developed by Alstom AQCS Service Solutions (now part of GE)
 - Continuous dissolved sulfite concentration measurement in a flowing, ambient pressure slipstream
 - Voltammetry method
 - Calibrated by comparing output to manual measurements
- Patented approach to use analyzer output as a set point for controlling ox air flow rate
- Requires analyzer on each absorber reaction tank

GE Commercial Sulfite Analyzer

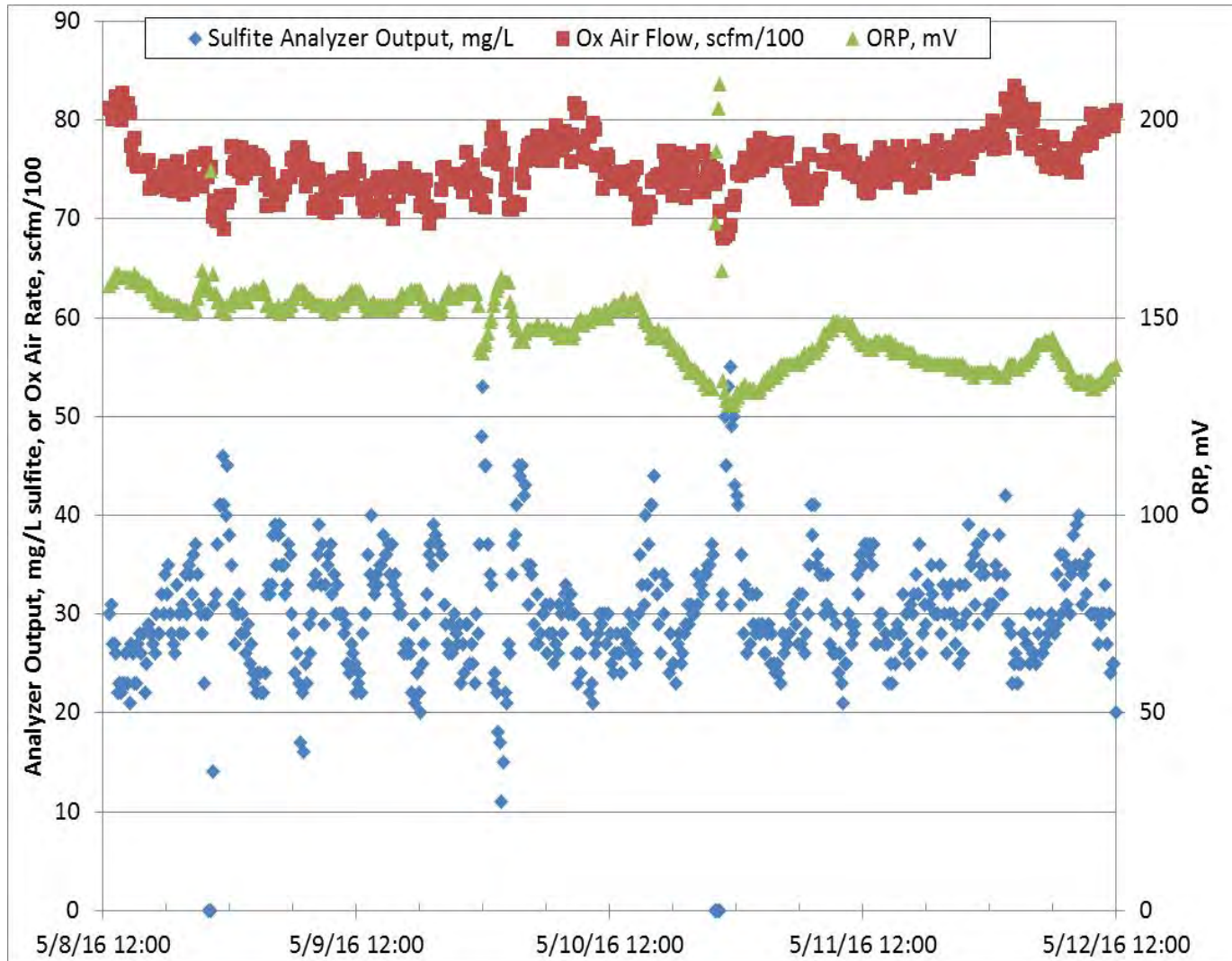
- Designed to operate in slurry service
 - “Wiper” rotates to keep probe tip clean
 - Weekly cleanup with soft brush to avoid solids buildup



Results for Sulfite Control of Forced Oxidation Air Rates

- Test conducted on 1 of 3 absorber modules on a 1300-MW unit firing medium-sulfur bituminous coal
 - Co-funded by utility and EPRI, in-kind support from GE
 - Spray towers with fixed sparger grids in reaction tanks
 - Tests conducted at $\geq 60\%$ load to avoid minimum air flow limits imposed by fixed sparger design
- Note that results similar to what follows could be achieved with Options 2 or 3 if adequate control of sulfite oxidation rate is achieved

Analyzer Output, Ox Air Rate, and ORP during Sulfite Control Operation

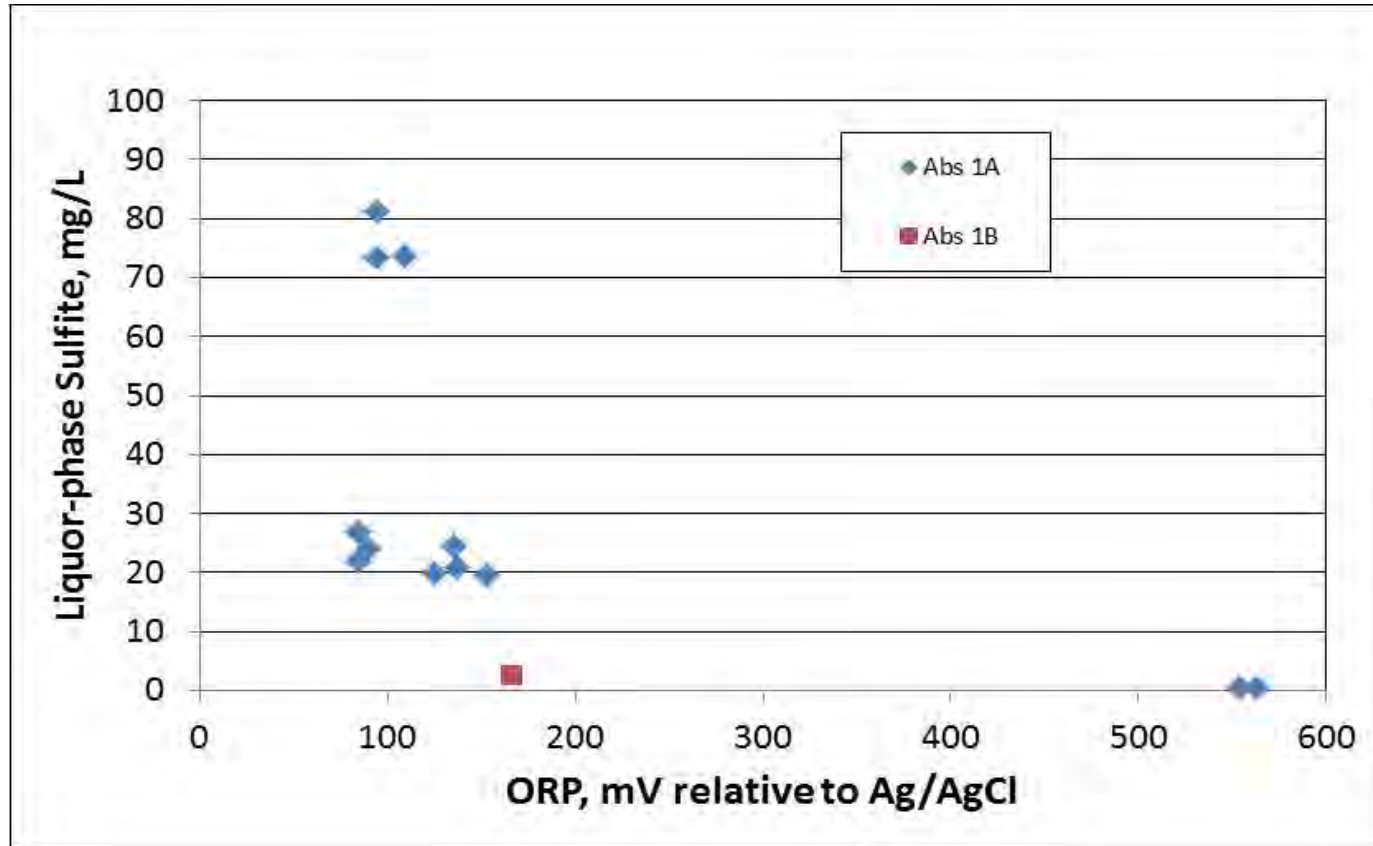


Analyzer Output versus Lab Measurements during Sulfite Control Operation

Date	SO ₃ ⁼ by IC, mg/L	SO ₃ ⁼ by Analyzer, mg/L	Relative % Difference
10/19/15	<1.1	Not in service	-
10/20/15	<1.1		-
5/11/16	20	27	30
5/11/16	21	29	32
5/11/16	20	33	49
5/12/16	25	35	33
6/15/16	81	79	3
6/15/16	73	79	6
6/15/16	74	78	5
2/16/17	22	24	8
2/16/17	24	23	6
2/16/17	27	27	4

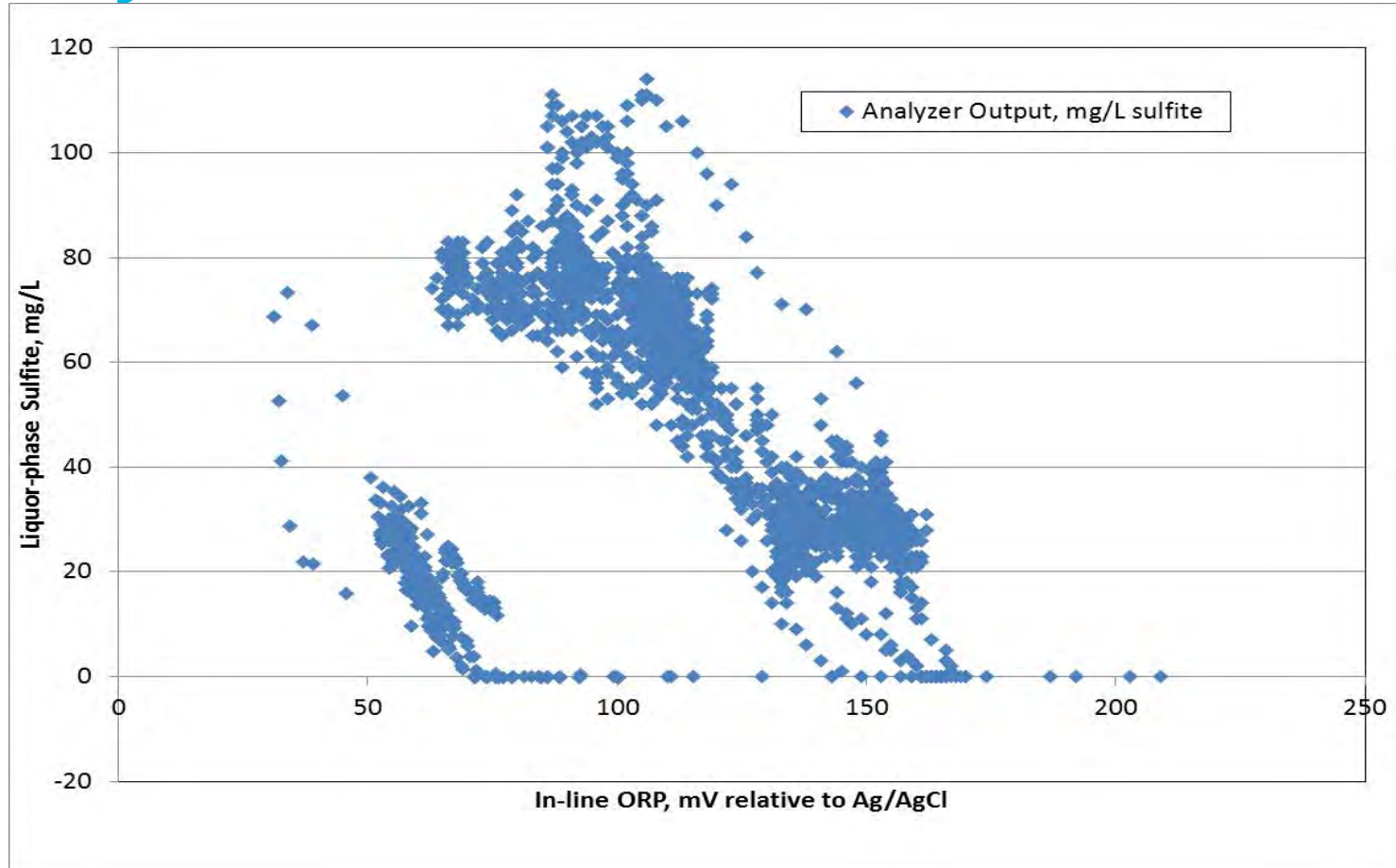
All sulfite values by analyzer reflect calibration from 10/21/15

Lab Result for Liquor-phase Sulfite vs. ORP by Hand-held Instrument



Note wide range of ORP values at 20-30 mg/L sulfite

Analyzer Result for Liquor-phase Sulfite vs. ORP by In-line Measurement



Controlling ORP at 150 mV would result in over oxidizing at some times

Absorber Hg Control Results

Test Condition	Inlet Hg Oxidation, %	Hg Removal across FGD	Hg Re-emission across FGD, % of inlet Hg ²⁺	Outlet Hg, lb/TBtu
Baseline, no sulfite control	98	60	38	1.0
Sulfite Control, 20-30 mg/L	97	98	0	0.2
	99	99	0	0.1
Sulfite Control, 70-80 mg/L	95	96	0	0.1

Test Absorber Average Hg Phase Partitioning Results

Condition	ORP, mV	Dissolved Hg, ng/L	Hg in slurry solids, µg/g	% of total Hg in slurry liquor	% of total Hg in slurry solids
Baseline, no sulfite control	560	75,000	0.17	70	30
Sulfite control, 20-30 mg/L	140	90	0.55	0.09	99.91
	90	50	0.55	0.05	99.95
Sulfite control, 70-80 mg/L	100	160	0.58	0.15	99.85
No sulfite control*, Nalco 8034+	170	20	0.55	0.02	99.98

*Sister absorber using Nalco 8034+ re-emission control additive

Test Absorber Average Se Phase Partitioning Results

Condition	ORP, mV	Dissolved Se, µg/L	Se in slurry solids, µg/g	% of total Se in slurry liquor	% of total Se in slurry solids
Baseline, no sulfite control	560	610	1.6**	67	33
Sulfite control, 20-30 mg/L	140	290	3.4**	29	71
	90	140	2.3	25	75
Sulfite control, 70-80 mg/L	100	340	2.8**	39	61
No sulfite control*, Nalco 8034+	170	150	2.7	24	76

*Sister absorber using Nalco 8034+ re-emission control additive

**Result is above MDL but below reporting limit, estimated result

Test Absorber Average Se Speciation Results

Condition	ORP, mV	Dissolved Se, µg/L	% Selenite	% Selenate	% Other Selenium Species
Baseline, no sulfite control	-	-	-	~99*	-
Sulfite control, 20-30 mg/L	90	140	93	6	1
Sulfite control, 70-80 mg/L	100	340	97	3	<1
No sulfite control,** Nalco 8034+	170	150	53	47	1

*Previous data from the same FGD system at baseline operation

** Sister absorber using Nalco 8034+ re-emission control additive

Test Absorber Average Total Nitrate/Nitrite Results

Condition	ORP, mV	Total NO ₃ ⁻ /NO ₂ ⁻ , mg/L	Apparent S/N species, mg/L as SO ₄ ⁼
Baseline, no sulfite control	560	16	80
Sulfite control, 20-30 mg/L	140	5	620
	90	5	NA
Sulfite control, 70-80 mg/L	100	2	260
No sulfite control*, Nalco 8034+	170	8	NA

Nitrate concentrations may be lowered by conversion to sulfur-nitrogen species

Test Absorber Average Mn Phase Partitioning Results

Condition	ORP, mV	Dissolved Mn, µg/L	Mn in slurry solids, µg/g	% of total Mn in slurry liquor	% of total Mn in slurry solids
Baseline, no sulfite control	560	50	22	1	99
Sulfite control, 20-30 mg/L	140	3800	3.5	86	14
	90	5600	4.1	88	12
Sulfite control, 70-80 mg/L	100	3700	4.7	81	19
No sulfite control*, Nalco 8034+	170	5000	7.1	79	21

*Sister absorber using Nalco 8034+ re-emission control additive

Mn becomes insoluble at highly oxidizing conditions; can scale on alloys of construction, exacerbate under-deposit corrosion

Potential Power Savings (estimates for controlling sulfite on all absorbers at host unit)

Parameter	50% to 100% Load, Full Ox Air Flow	100% Load, Sulfite Control	50% Load, Sulfite Control
Air to 3 Absorbers, SCFM	30,775	21,525	15,375
No. of Operating Air Blowers	2	2	1
Total Blower Power, kW	1910	1492	955
Power Savings, kW	-	418	955

Summary

- Many benefits from controlling forced ox air flow to avoid over-oxidizing conditions
 - Improved Hg capture, less need for PAC injection or re-emission additives
 - Lower concentrations of ELG constituents in wastewater
 - Less tendency for under-deposit corrosion of alloys of construction
 - Less power consumption by forced ox blowers, depending on blower type and system configuration

Summary (continued)

- Three options discussed for controlling ox air rates:
 - **ORP control:** can be imprecise, other redox reactions impact probe readings, possible patent issues
 - **Feed forward algorithms:** empirical, may have to be tuned as process changes occur
 - **In-line sulfite analyzer control of air rate:** direct control of sulfite oxidation rate; down side is cost of analyzer, particularly for multi-module systems
- Any control option may require modifications to ox air system to improve turndown

Questions or Comments?

Gary Blythe

(512) 419-5321

Gary.Blythe@AECOM.com