

# **REINHOLD ENVIRONMENTAL<sup>®</sup>**



## **2026 Reinhold/PCUG Round Table Presentation**

Hosted by TVA, Southern Company and Vistra  
in the Sonesta Nashville Airport Hotel, Nashville, TN  
on June 22-23, 2026

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# *From Why to How: A Hydrated Lime DSI Primer*

*Curt Biehn*

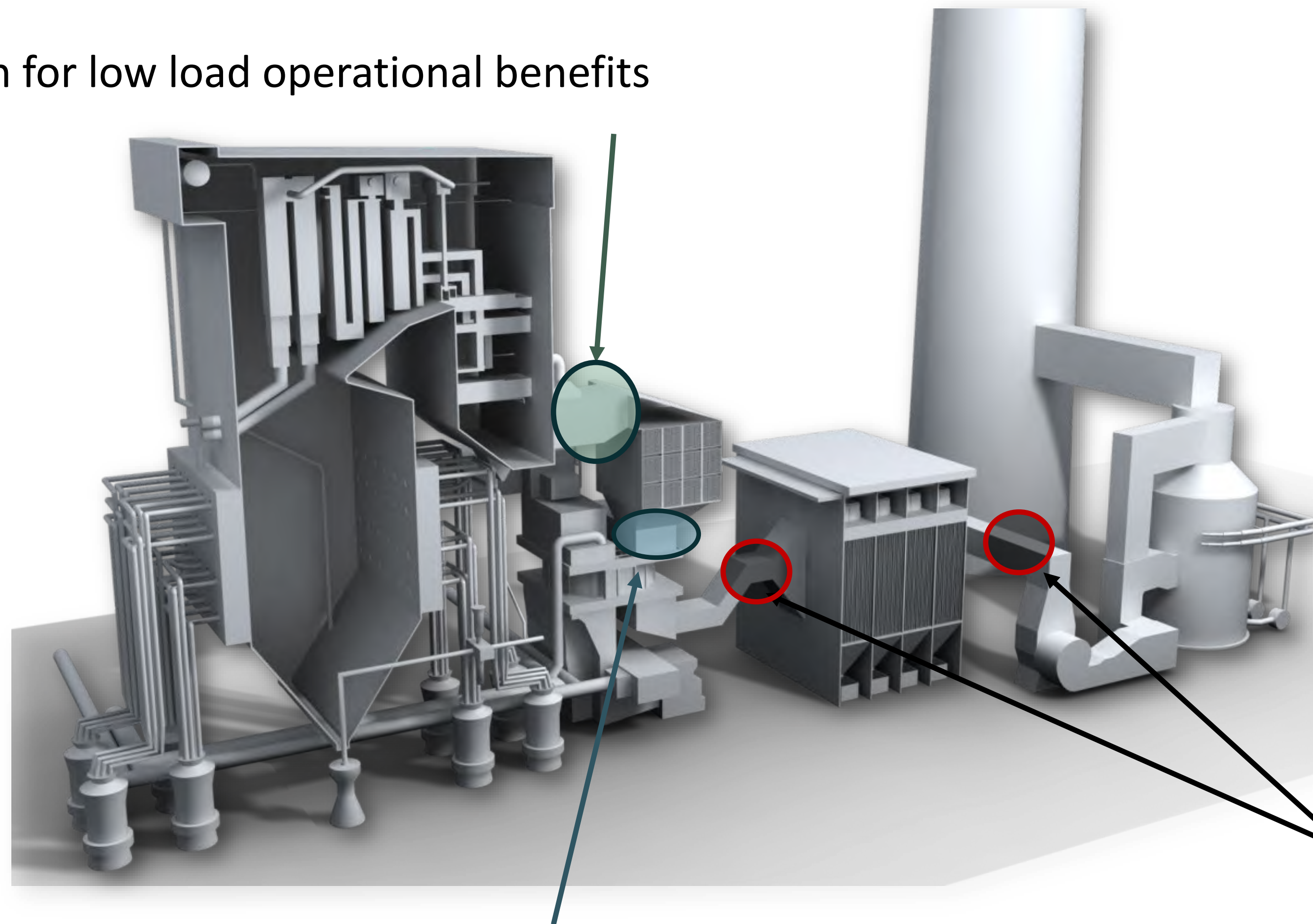
*Workshop 25 - Reinhold Conference Round Table  
June 23, 2026*



# *Dry Sorbent Injection Using Hydrated Lime*



Pre-SCR injection for low load operational benefits



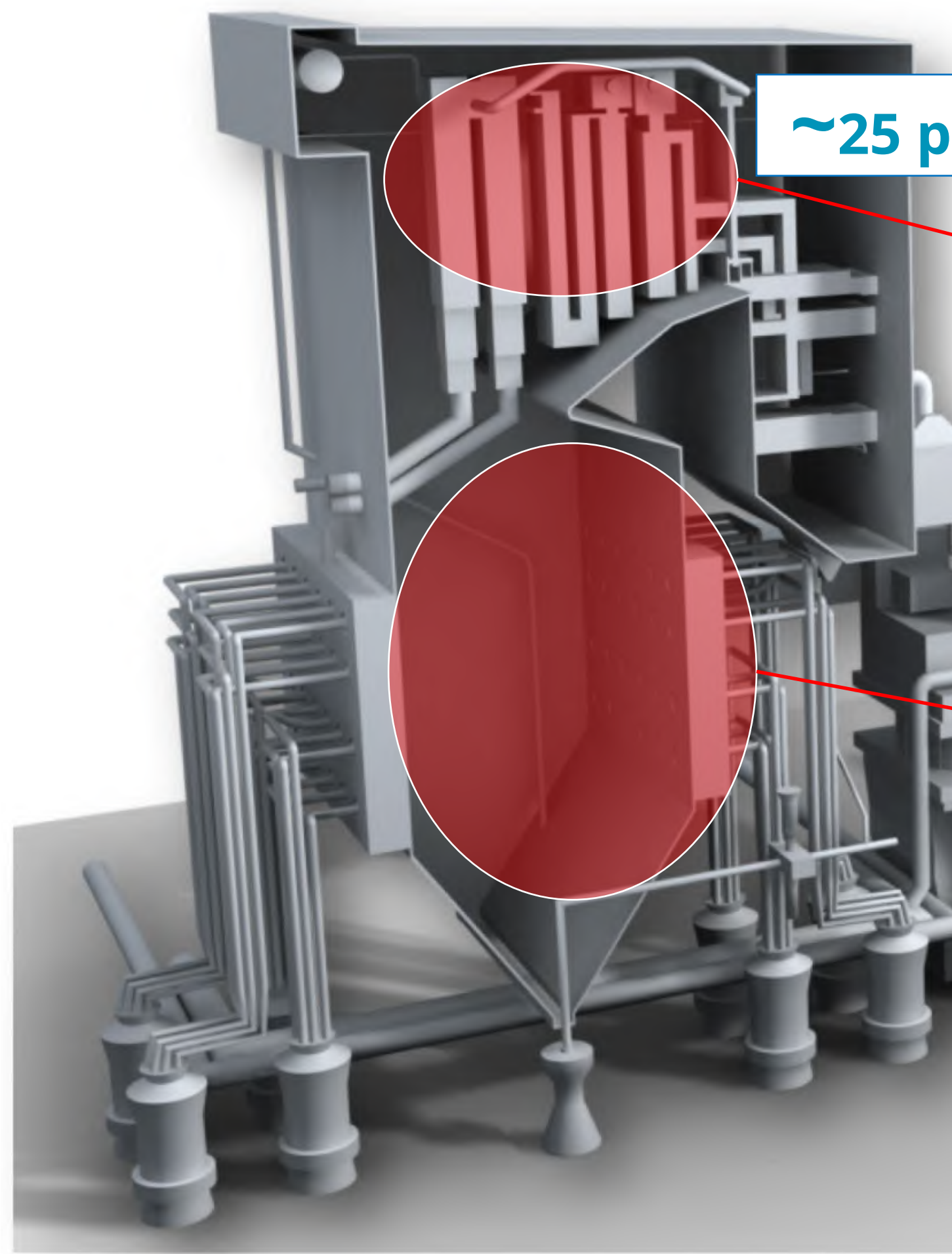
Pre-Air Preheater (APH) injection for APH cleanliness and other operational benefits

Post-APH injection to meet regulatory requirements

*Why are we  
using Hydrated  
Lime?*



# *SO<sub>3</sub> Generation in the Furnace*



~25 ppm SO<sub>3</sub>

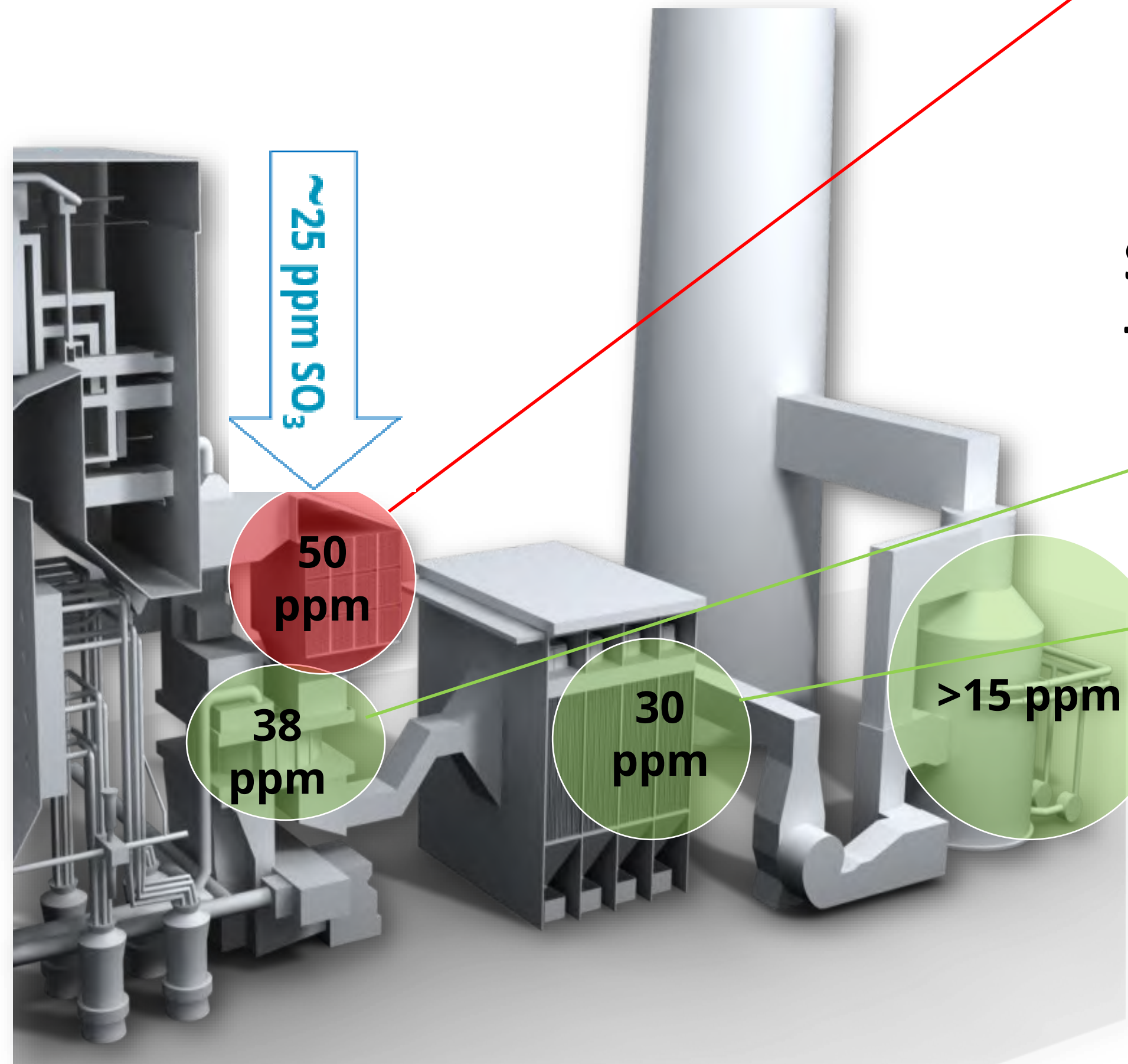
**Most Furnace SO<sub>2</sub>:SO<sub>3</sub> conversion happens in the convective zone in the presence of iron, oxygen and suitable temperature**

**SO<sub>2</sub> is formed during coal combustion at the burner and in the fire ball.**

**Small amount of SO<sub>3</sub> generated; excess O<sub>2</sub> in the furnace is typically low**

**Rule of Thumb is that 1% of the Furnace SO<sub>2</sub> converts to SO<sub>3</sub>**

# *SO<sub>3</sub> Fate Downstream of the Furnace*



**SCR increases SO<sub>3</sub>**

- Catalyst (type/layers/activity), ammonia, and temperature are major influencers

**SO<sub>3</sub> converts to H<sub>2</sub>SO<sub>4</sub> downstream of SCR depending on temperature and moisture in flue gas**

**Lose 20-25% of SO<sub>3</sub> across the Air Preheater**

**Can lose 10-25% H<sub>2</sub>SO<sub>4</sub> in ESP/BH**

**Can lose 10-50% H<sub>2</sub>SO<sub>4</sub> in Wet FGD**

**Loss of SO<sub>3</sub>/H<sub>2</sub>SO<sub>4</sub>**

- Deposition on flue internals (corrosion) and ash
- Reaction with ammonia to form ammonium bisulfate

# *How Much Sulfuric Acid Mist Needs Mitigated?*



- Eliminate visual blue plume (~5-8 ppm  $\text{SO}_3$  at the stack)
- Eliminate the  $\text{SO}_3$  created from installation of SCR
- Limit applied by a regulatory authority
  - Stack testing on a frequency
  - Stack emissions tracked by a Continuous Emissions Monitor

# Modern Era of Dry Sorbent Injection for Sulfuric Acid Mist Control

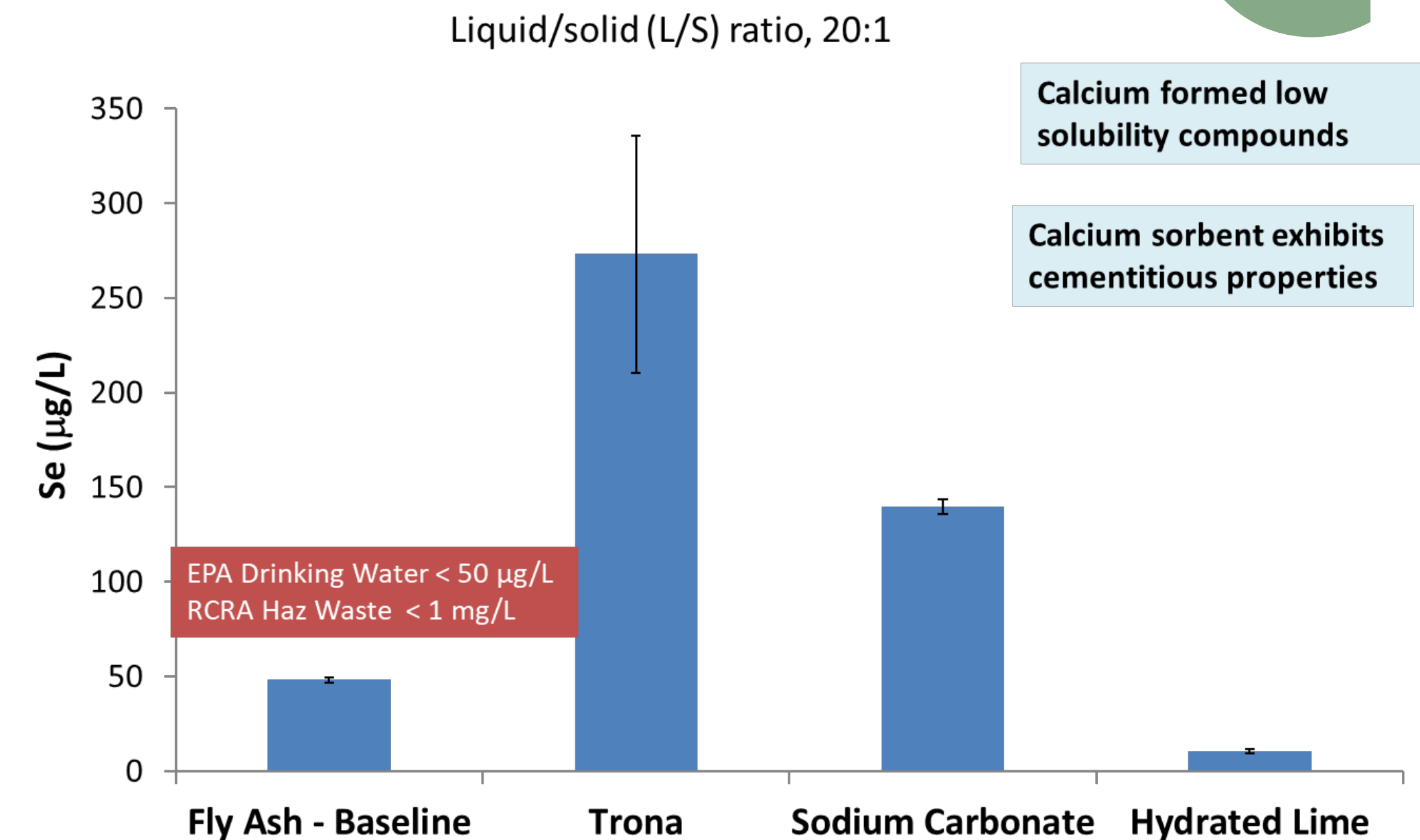


- Problem created from solving two problems
  - SCRs ( $\text{NO}_x$ ) + Wet Scrubbers ( $\text{SO}_2$ ) + High Sulfur Coal = Stack Sulfuric Acid Mist
  - Blue plume touchdown on local communities
- Required rapid resolution – neutralize with base
  - Trona
  - Sodium Bisulfate Solution (SBS)
  - Hydrated Lime
- Utilities initially successful with sodium-based sorbents

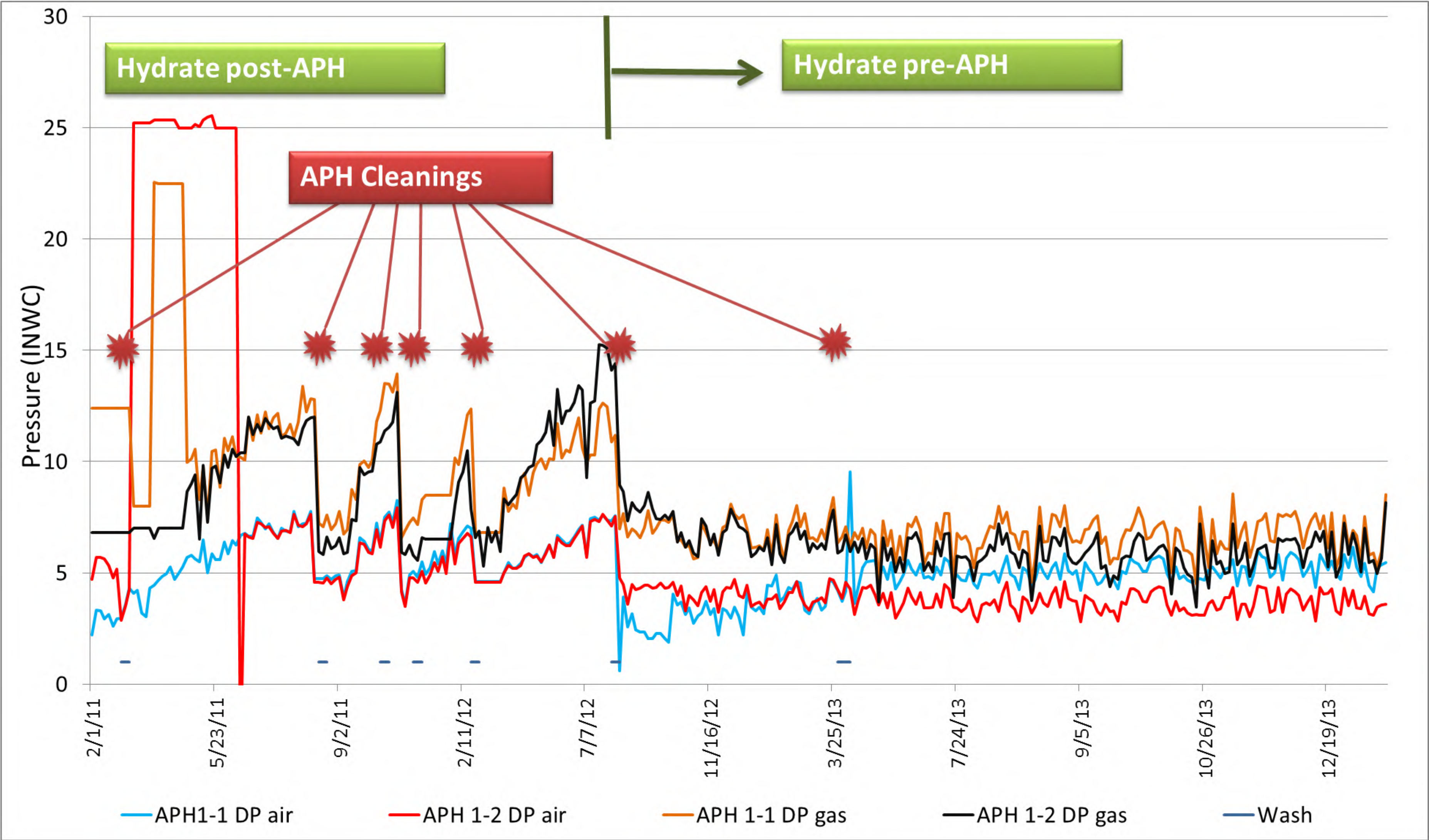


# How Did Hydrated Lime Flip the Field

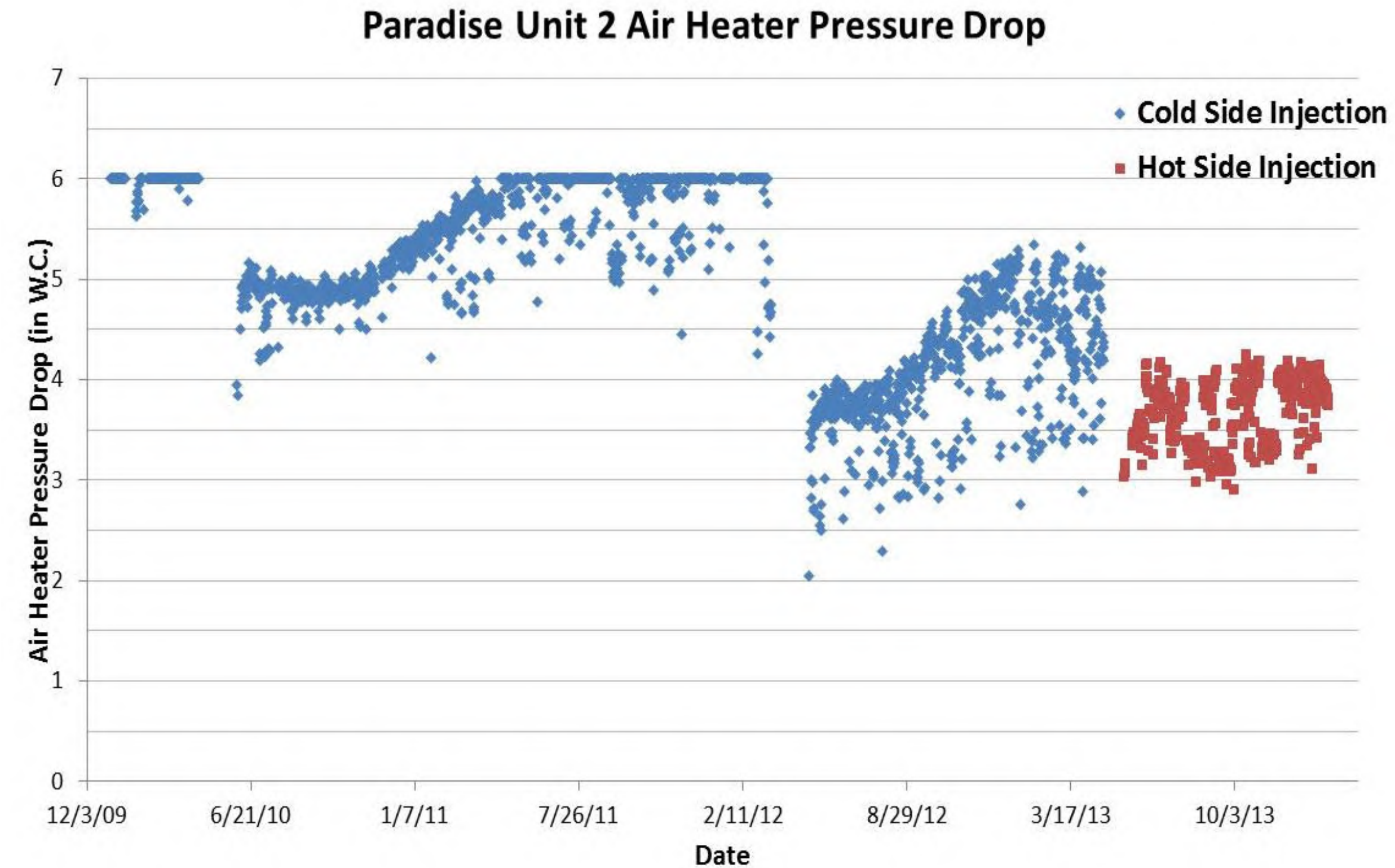
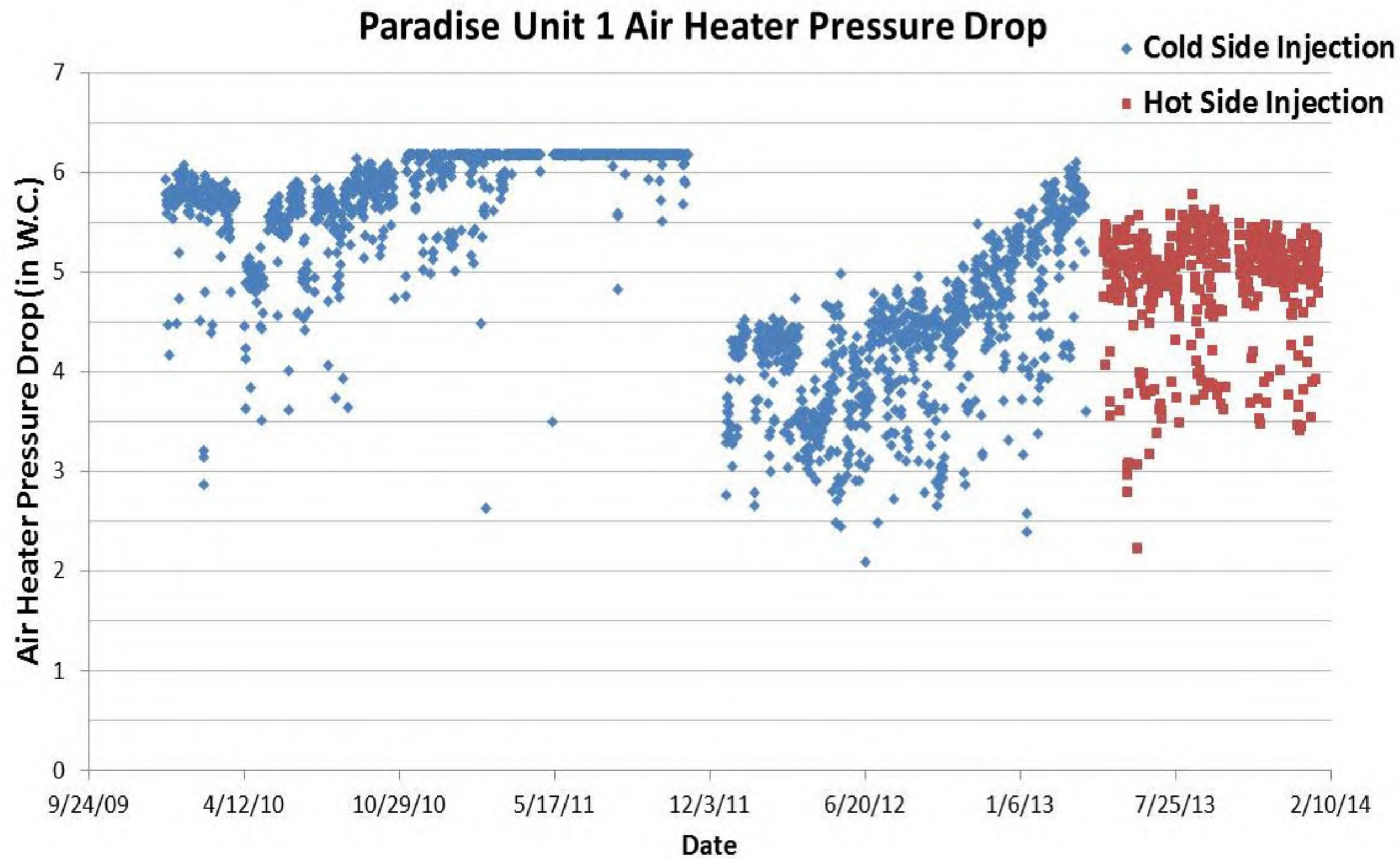
- Improved performance
  - Better entry-level products
  - Enhanced hydrates
- Fewer or less stringent ancillary issues
  - No problematic byproducts in ducts
  - Sellable ash
  - Relatively fewer conveying issues
- Advantages over sodium sorbents
  - Multiple hydrated lime sources in regions where  $\text{SO}_3$  emissions are an issue
  - Operational benefits benefit beyond pollution control
    - Pre-APH injection



# Hydrated Lime Pre-APH – Effects on APH Dp



# Pre-APH Hydrate Benefits at TVA Paradise



Jan 2011 – Mar 2013: over **570,000 MWh** lost due air heater fouling from both units.

Began hot side injection Apr 2013, **0 MWh** were lost due air heater fouling (Feb 2014 report)

# *Pre-SCR Injection of Hydrate*

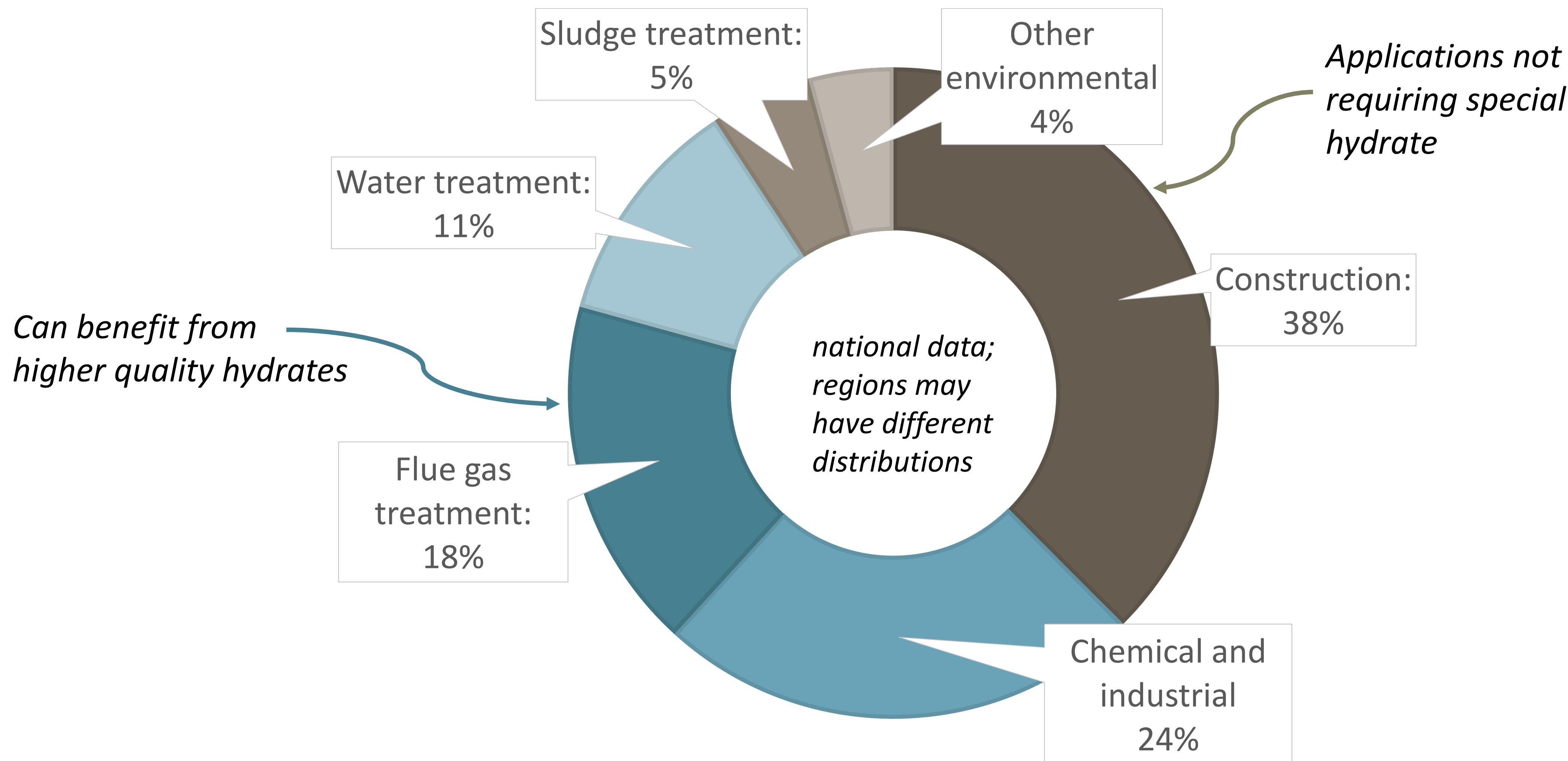


- Reduce the Minimum Operating Temperature
  - Interaction of  $\text{SO}_3$  deposition onto SCR catalyst sets minimum load
  - Neutralize  $\text{SO}_3$  -> Reduced dew point
  - Hydrate or calcium sulfate should not chemically degrade catalyst
- Lower MOT = Reduced Minimum Load
  - Fuel cost savings while awaiting load ramp
  - Reduce  $\text{CO}_2$  emissions
- Typically need second hydrate injection point to capture  $\text{SO}_3$  generated in SCR

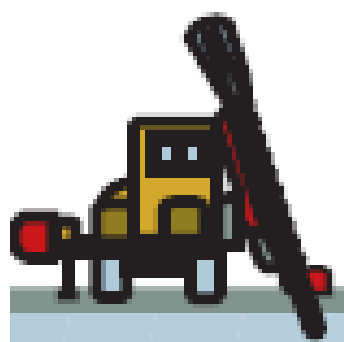
# USGS – Survey of Hydrated Lime Production in US



U.S. Hydrated Lime Markets - 2023



# Quicklime Production (Calcium Oxide)



 *Drilling & Blasting  
Limestone  
(Calcium Carbonate)*



Preheating  
Zone

Calcining  
Zone

Cooling Zone



 *Quicklime (Calcium Oxide)*



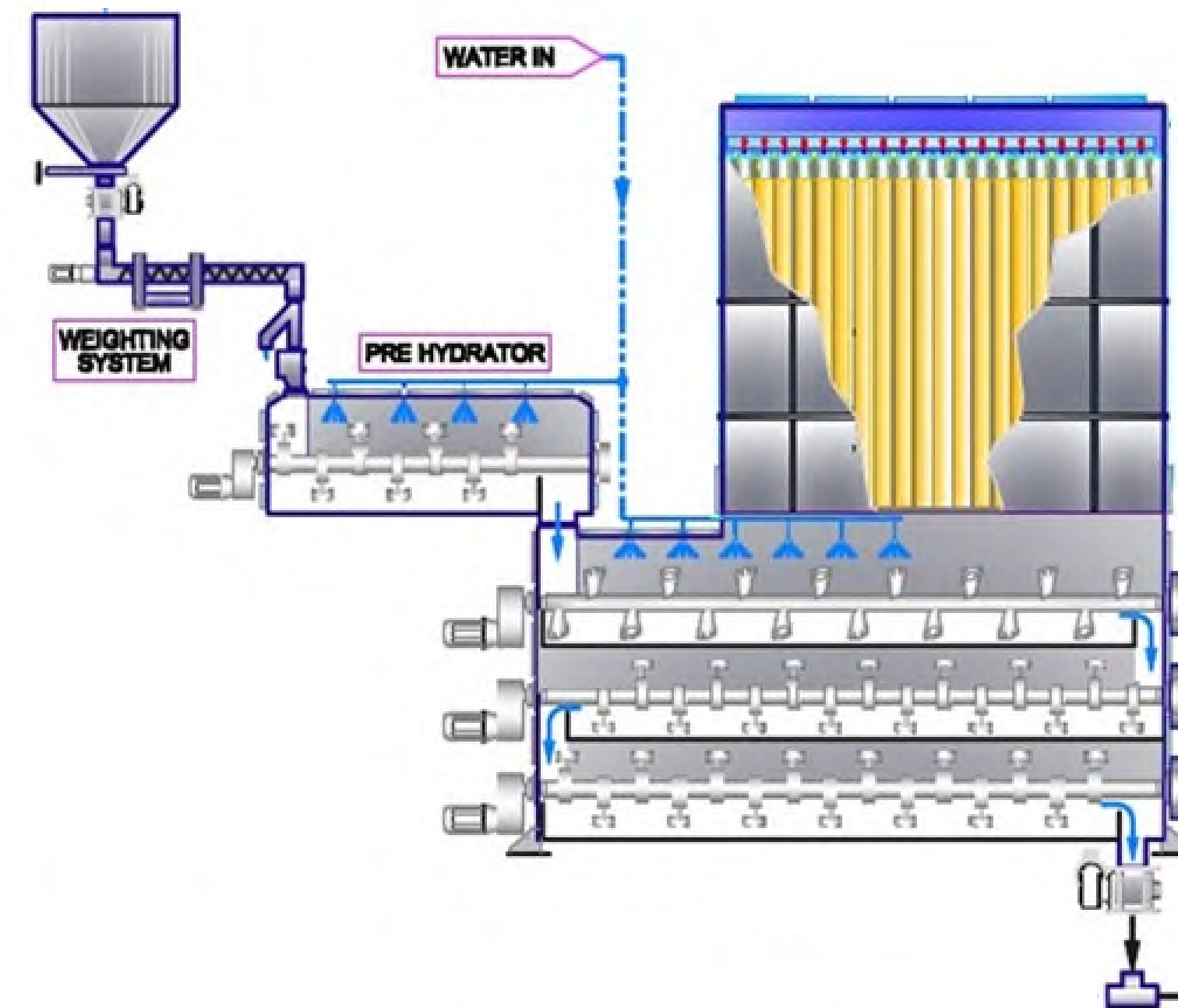
# Hydrate Production(Calcium Hydroxide)



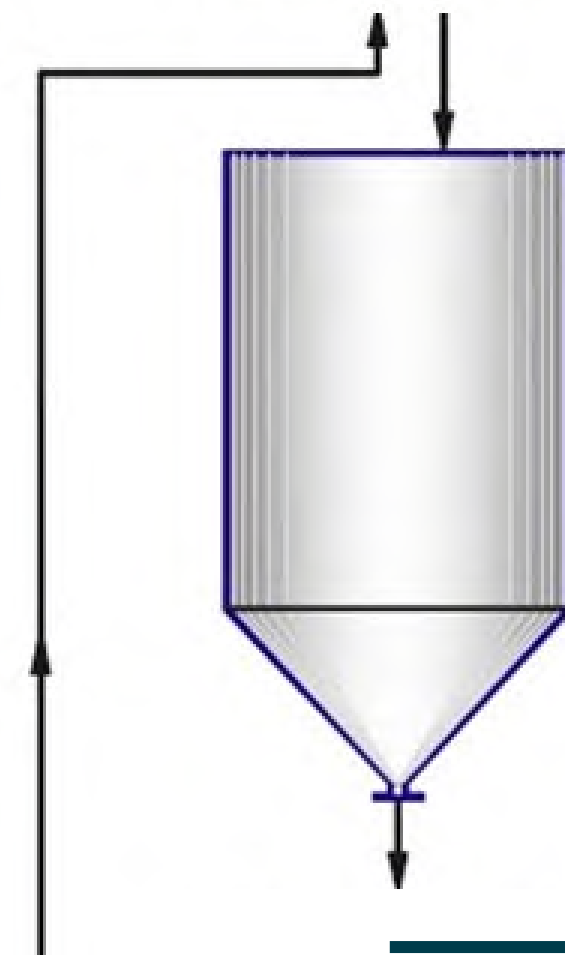
 Quicklime  
(Calcium Oxide)



 Hydration\*



 Refinement



Hydrated Lime  
(Calcium Hydroxide)



# What Makes a Hydrated Lime “Enhanced”

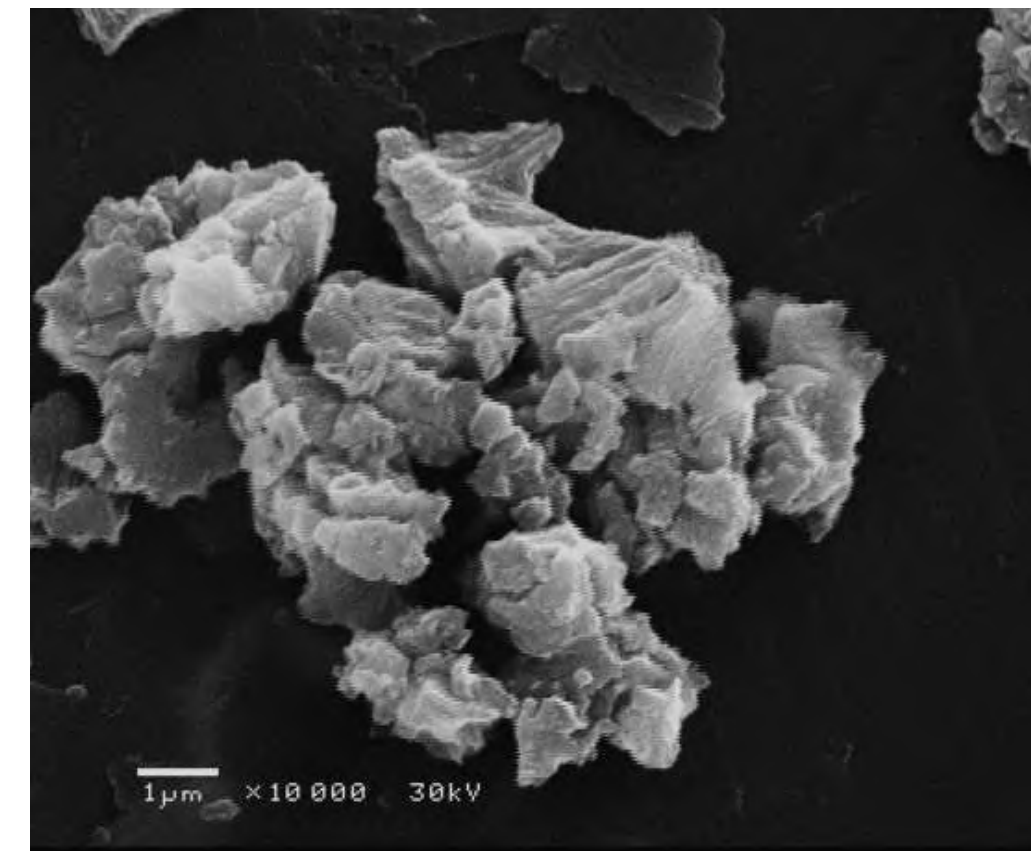


Lime supplier has **modified the manufacturing process to consistently** produce a hydrated lime that has **more active sites for neutralization of acids**

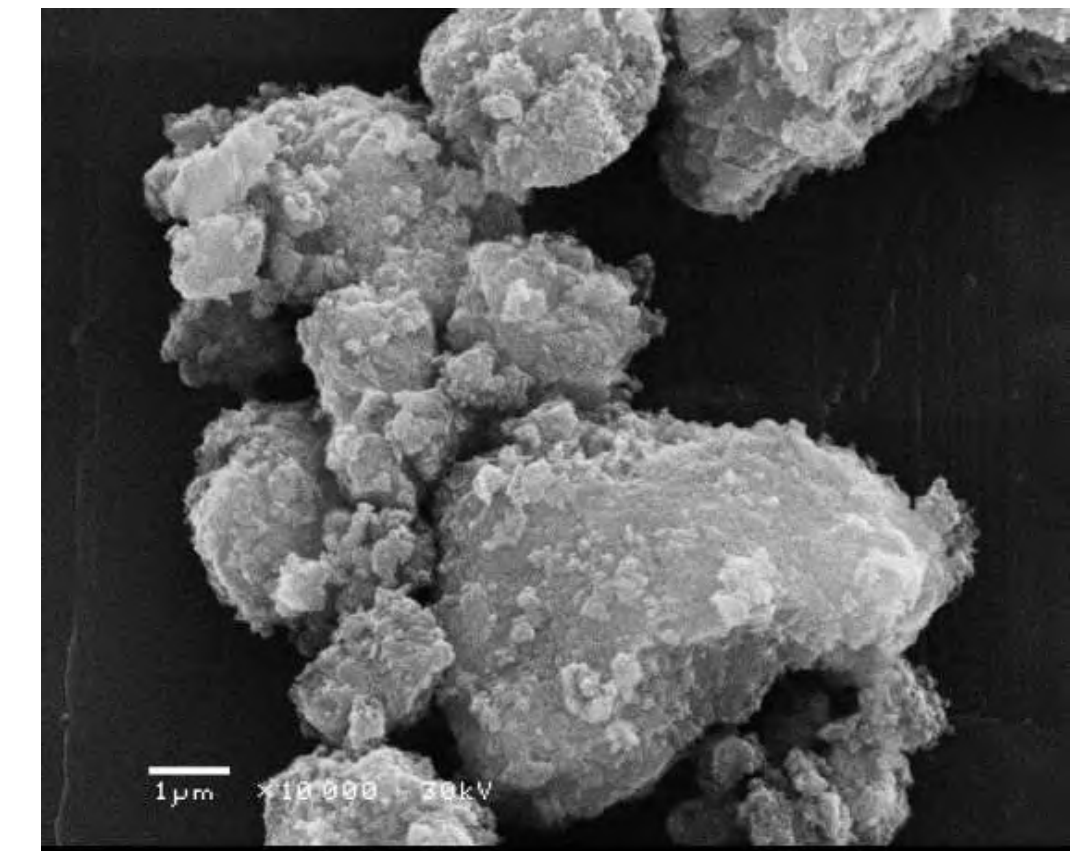
Think in terms of “effective surface area”

*J.A.H. Oates, “Lime and Limestone”*

1. The specific surface area (BET)
2. Total volume and size of pores
3. Particle size
4. Degree of agglomeration



*Enhanced hydrate*



*Standard hydrate*

*Enhanced hydrates are patented/proprietary technology  
Comparing suppliers solely on specifications is not simple  
Proof of performance comes in plant evaluations*

# *Benefits of Enhanced Hydrated Lime*

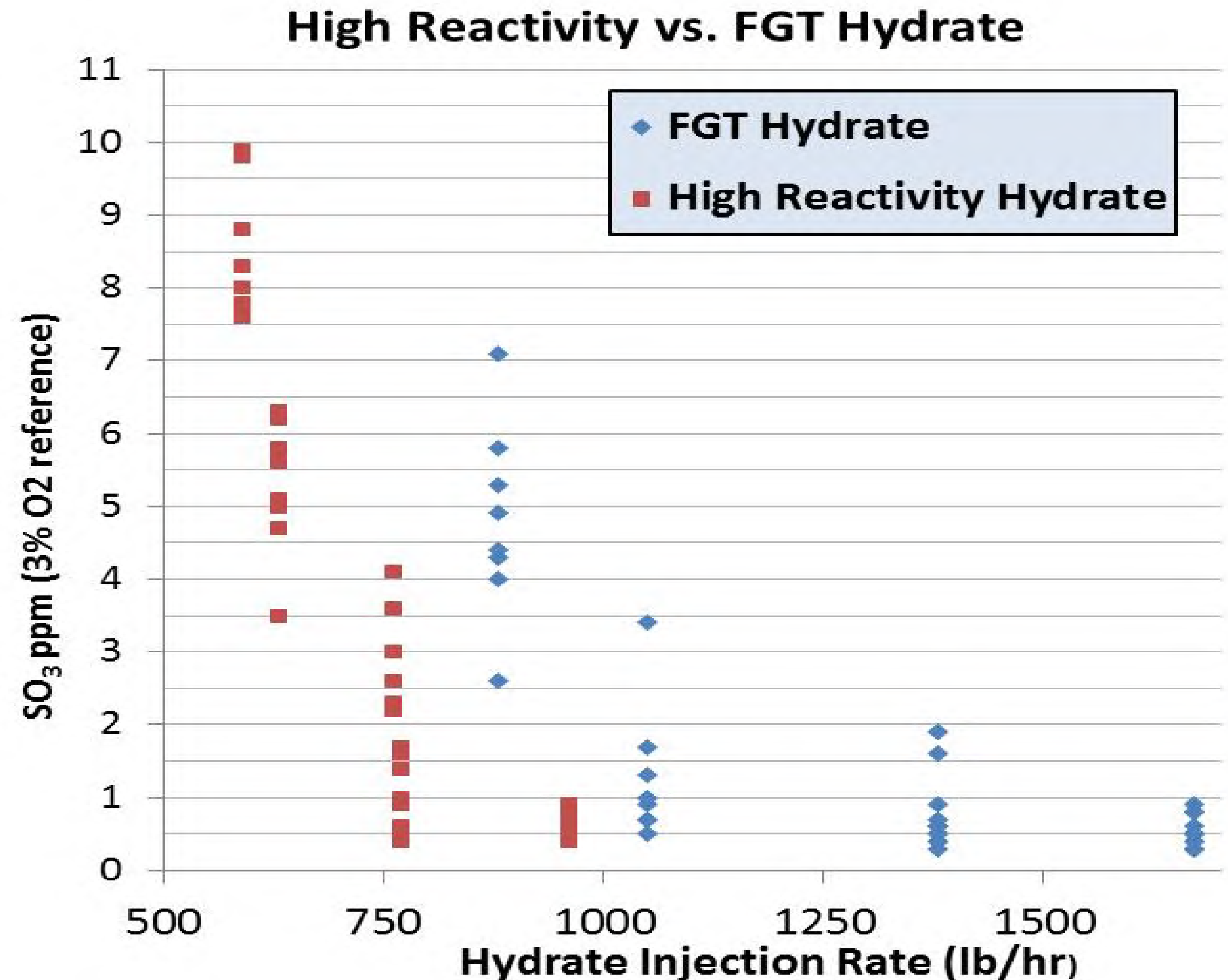


- Reduced emissions of  $\text{SO}_2$ ,  $\text{SO}_3$ , and HCl
  - Lower annual delivered hydrate costs while maintaining existing emission levels
- Flexibility:
  - Higher sulfur or chloride fuel
  - SCR operations to maximize  $\text{NO}_x$  reduction
  - Ability to control emissions with more challenging flue gas
- Reduce truck traffic and potential safety exposures during product deliveries
- Less ash
- Increase # days of sorbent storage

# FGT vs. High Reactivity Hydrate



- Both hydrates reduced  $\text{SO}_3$  by **94%-98%** across the APH
  - FGT = 1,000-1,100 lb/hr
  - HRH = **750-800 lb/hr**
- Acid dew-point reduction from 300°F to ~275°F



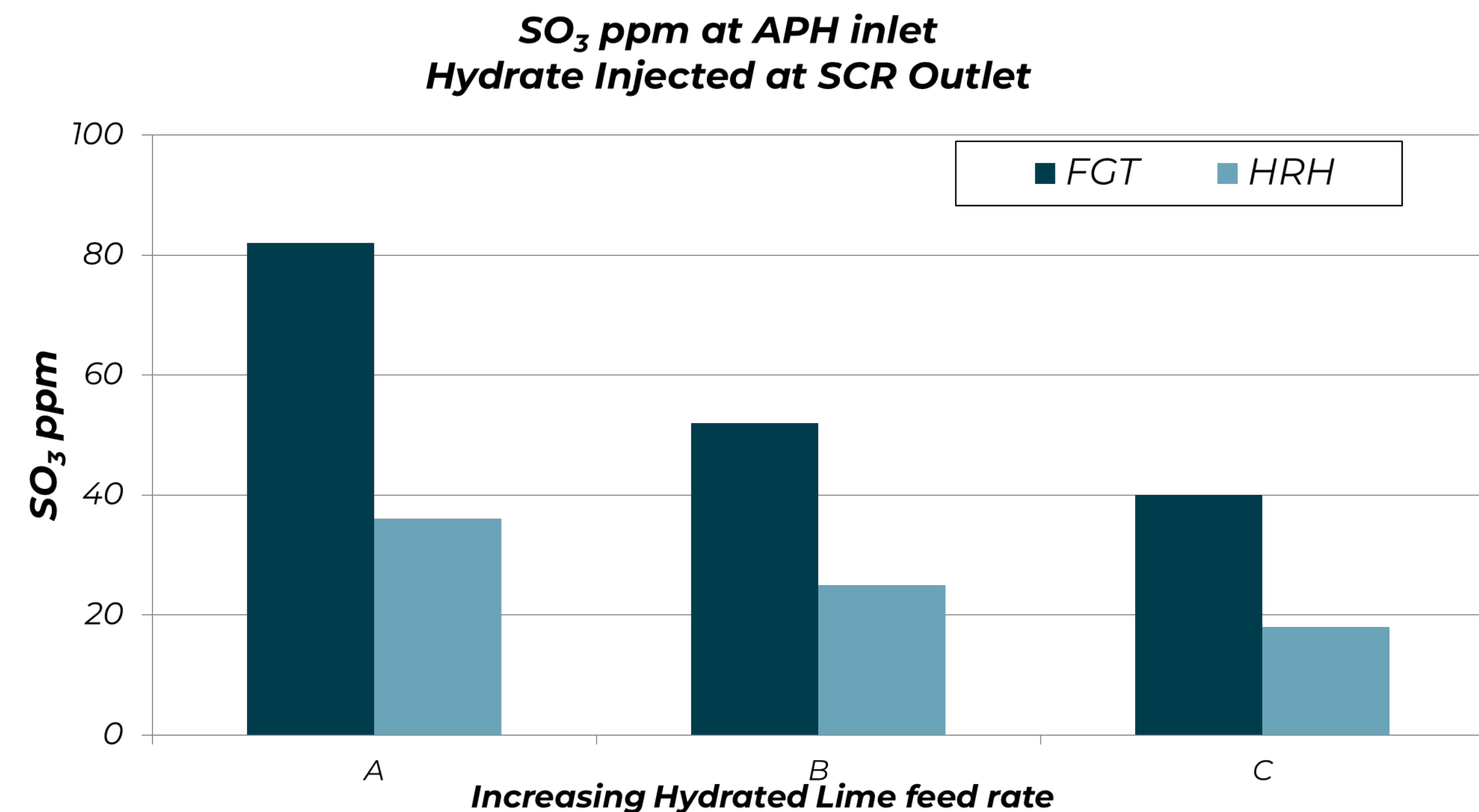
# HRH Works Better in a Tight Reaction Window



Utility desired high  $\text{SO}_3$  capture at Air Preheater inlet so they evaluated HRH versus their existing hydrate, FGT (Flue Gas Treatment)

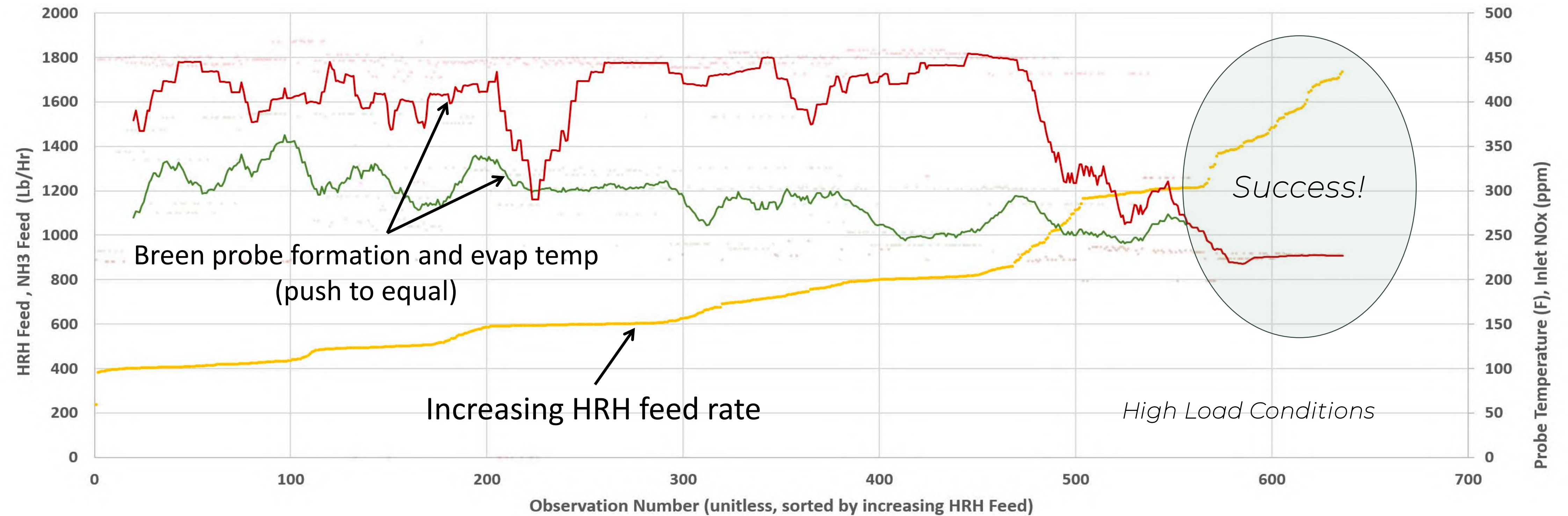
HRH reduced  $\text{SO}_3$  significantly compared to FGT hydrate

Customer had confidence the high reactivity sorbent would better prevent APH buildup



*Understand the in-flight capture of your hydrated lime*

# HRH Feed Rate + Condensable Formation Temperature Relationship



- HRH pre-SCR injection rate equivalent to trona post APH.
- APH diff pressure stabilized / ID Fan power consumption reduced / Soot blowing frequency minimized / Steam coil usage cut in half
- Marketable fly ash

# DSI Conveying System Components



*Feed Bin*



*Convey Air*



*Feeder*



*Convey Pipe*



*Splitter*

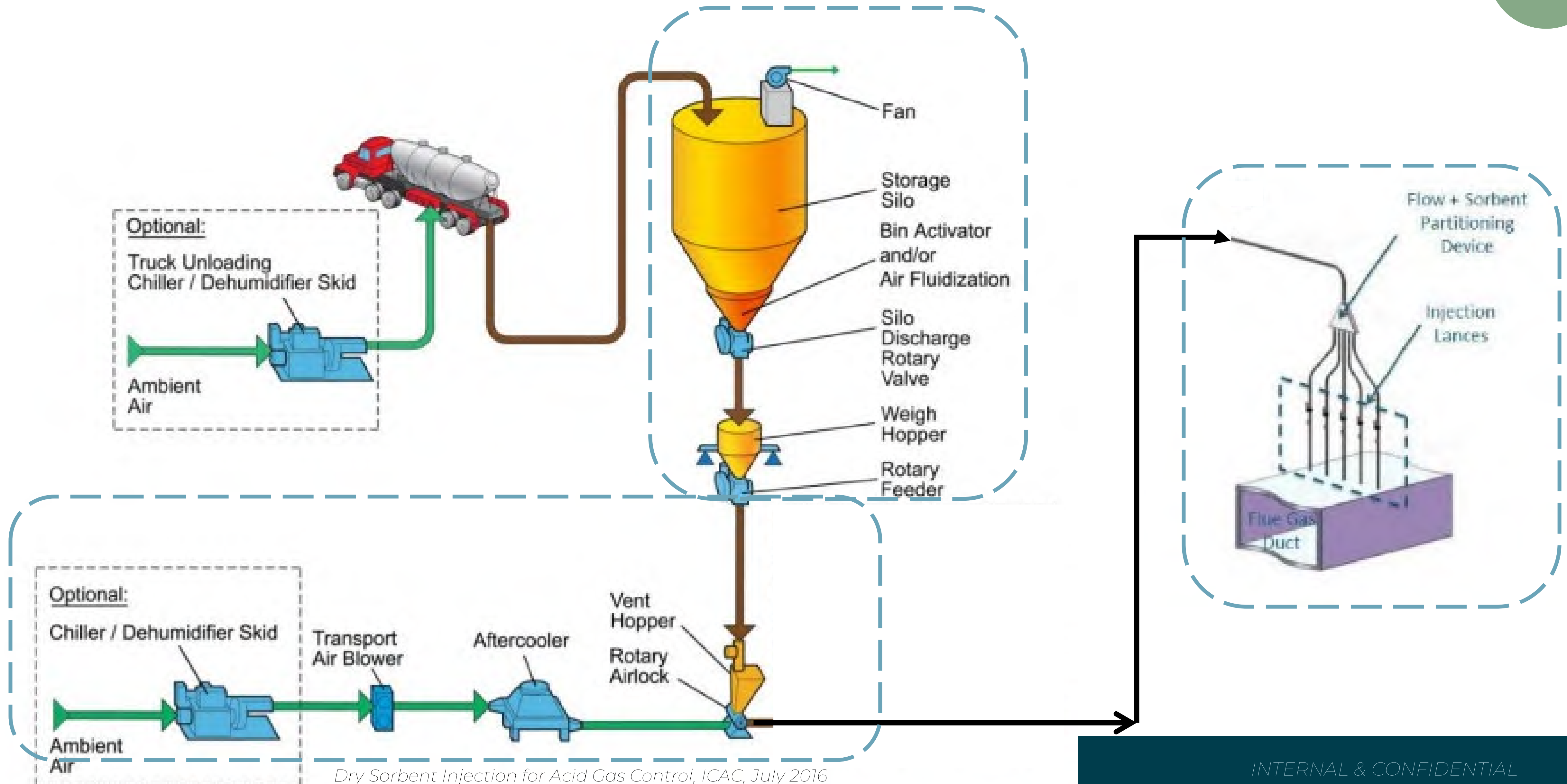


*Injection*



*Also used: dehumidifier, chiller/air-air heat exchanger, in-duct mixing devices, high dispersion lance tips*

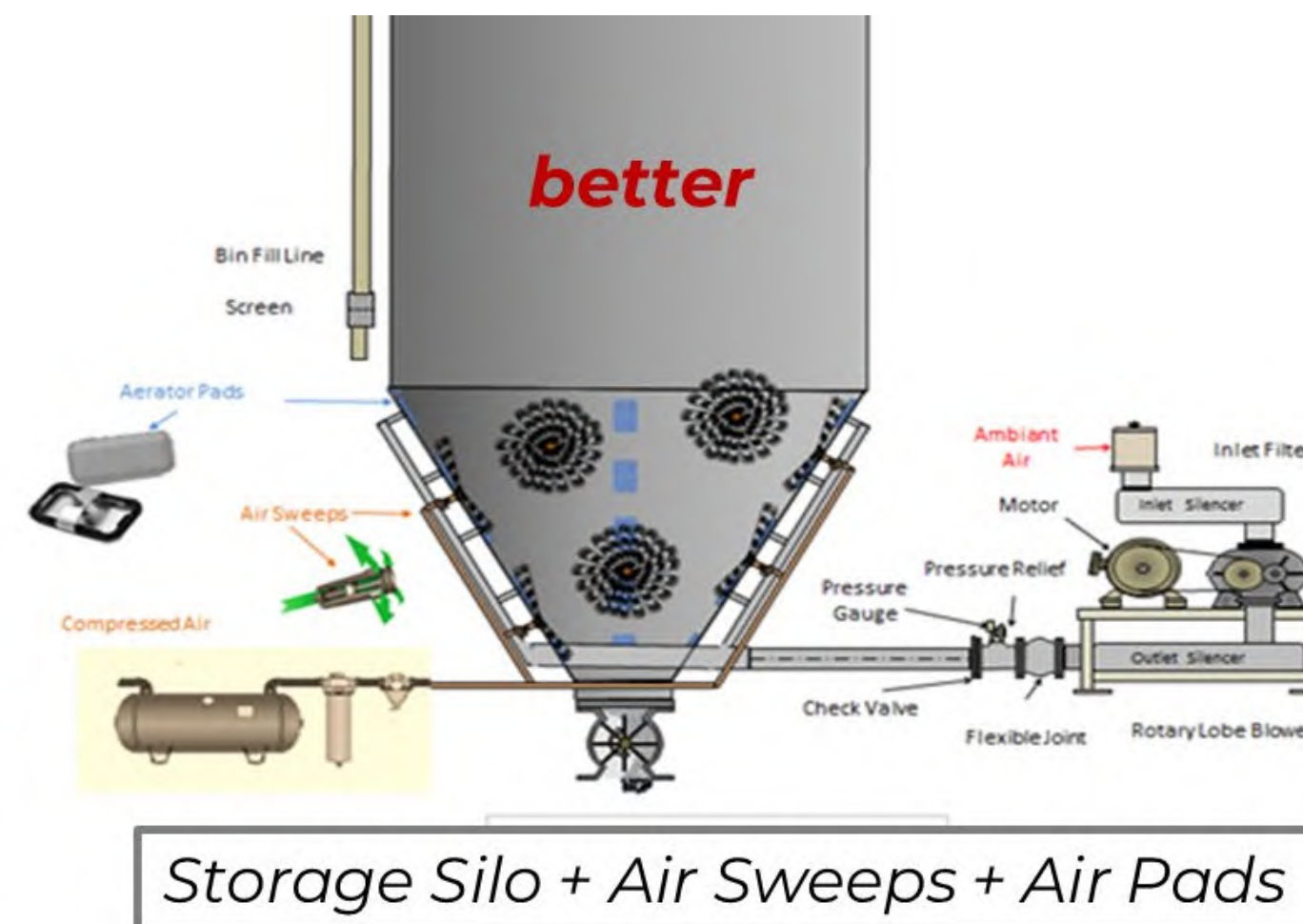
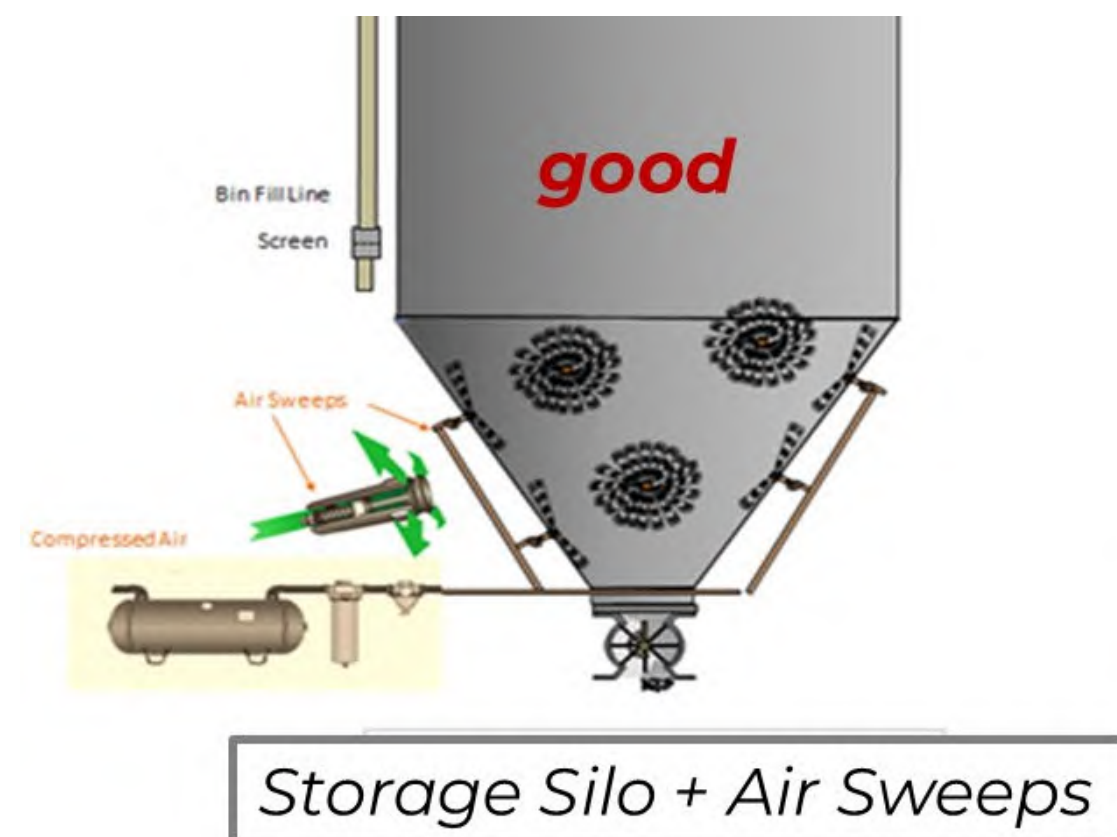
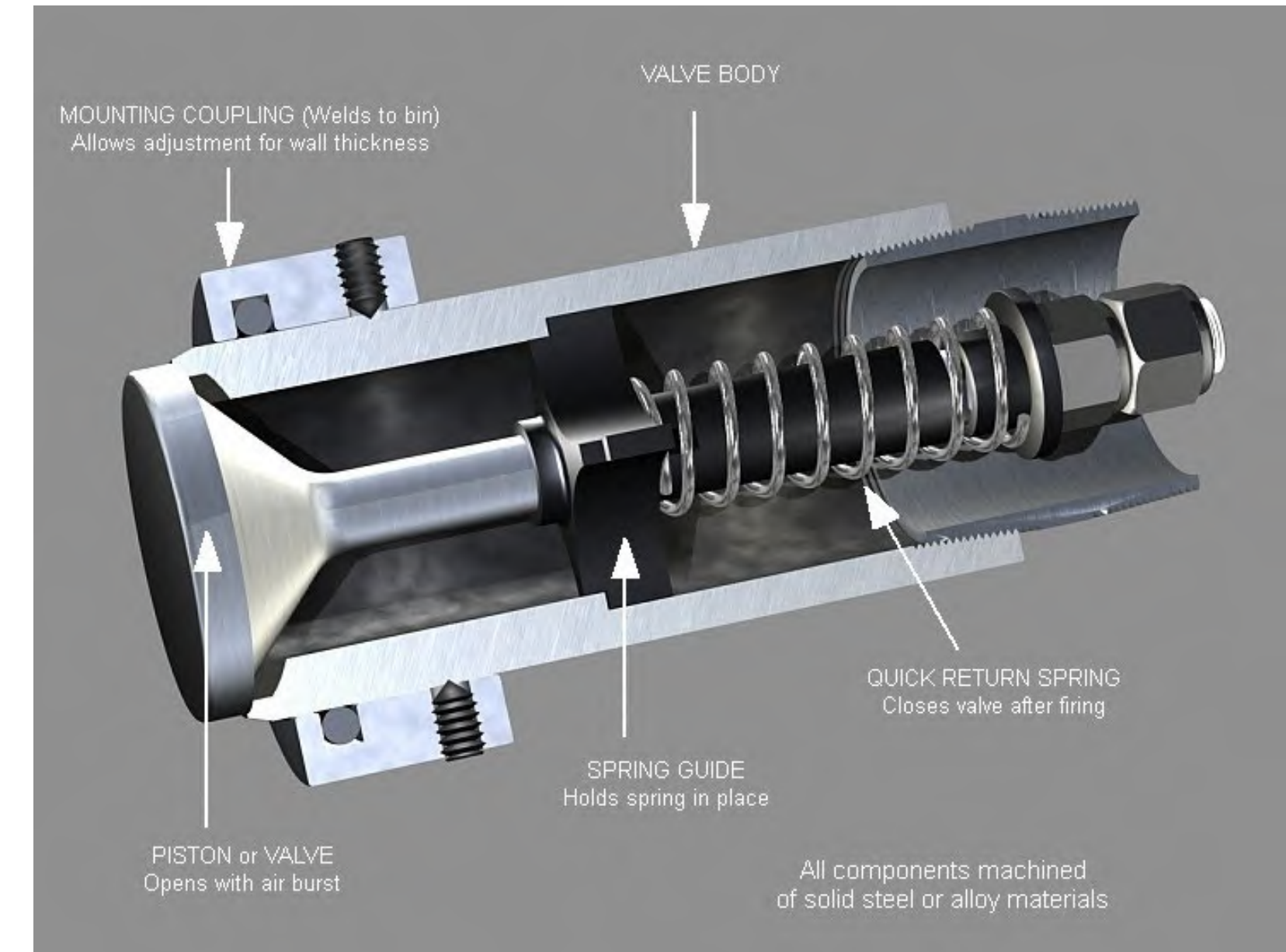
# DSI System



# Storage Silos



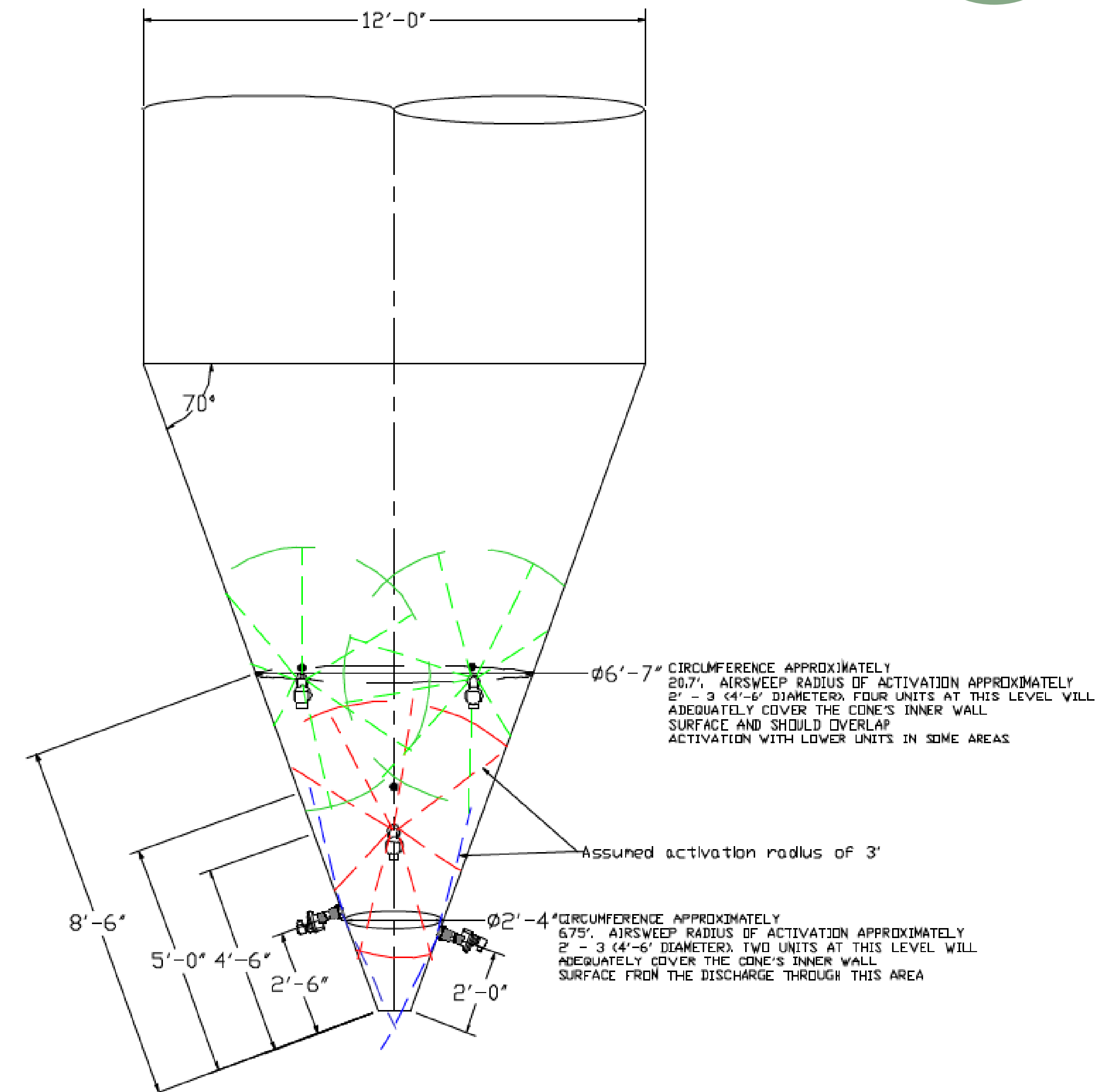
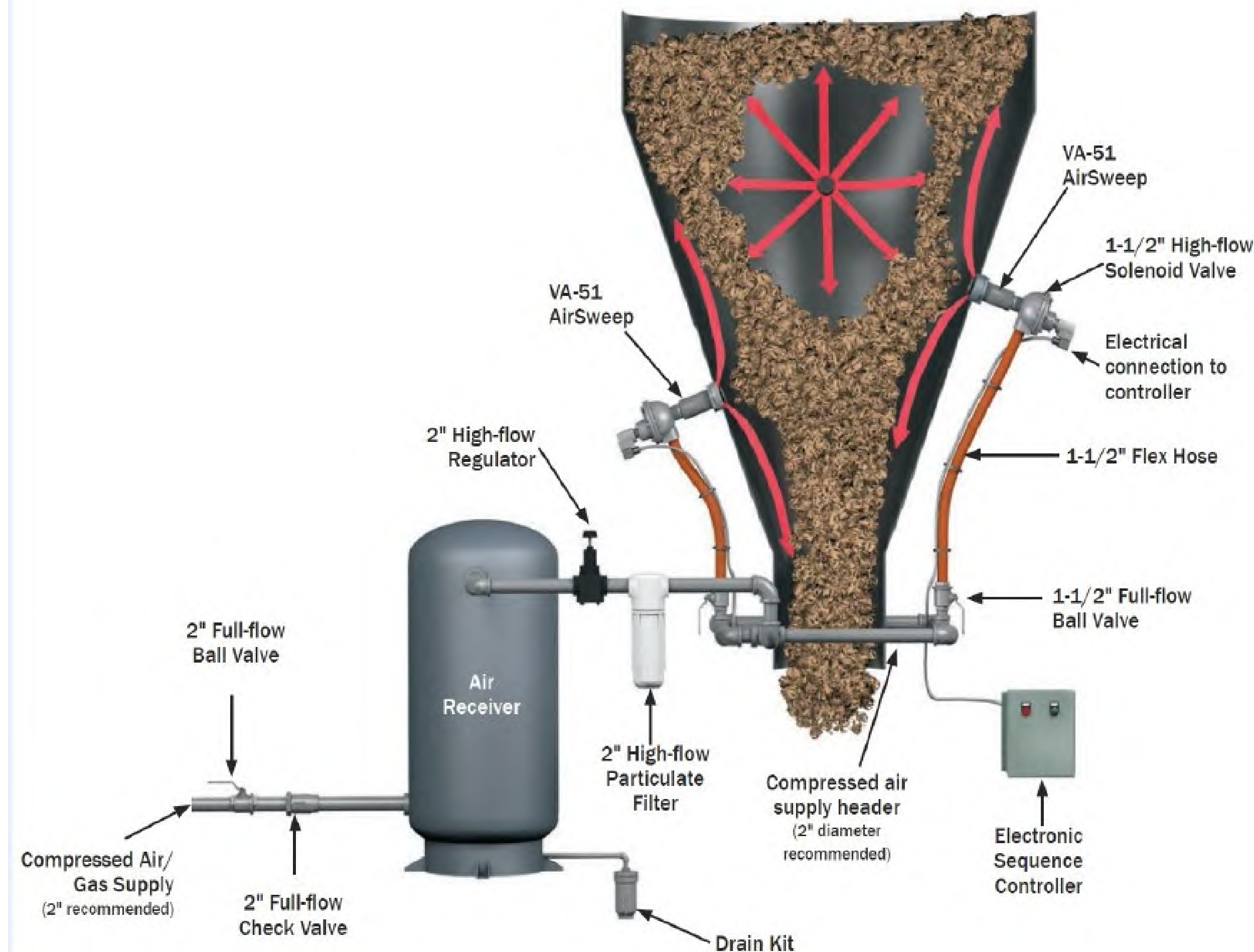
- Silo size to hold at least two truckloads (loose bulk density 20-25 lb/ft<sup>3</sup>)
- Level transmitter –
  - Radar or guided radar level detector
  - Capacitance detector for High/Low levels
- Dust collector – bag, not cartridge
- 60° Cone
- Fluidization
  - Air Sweeps + Air Pads > Air Sweeps >> Air Pads >> Live Bottom bins





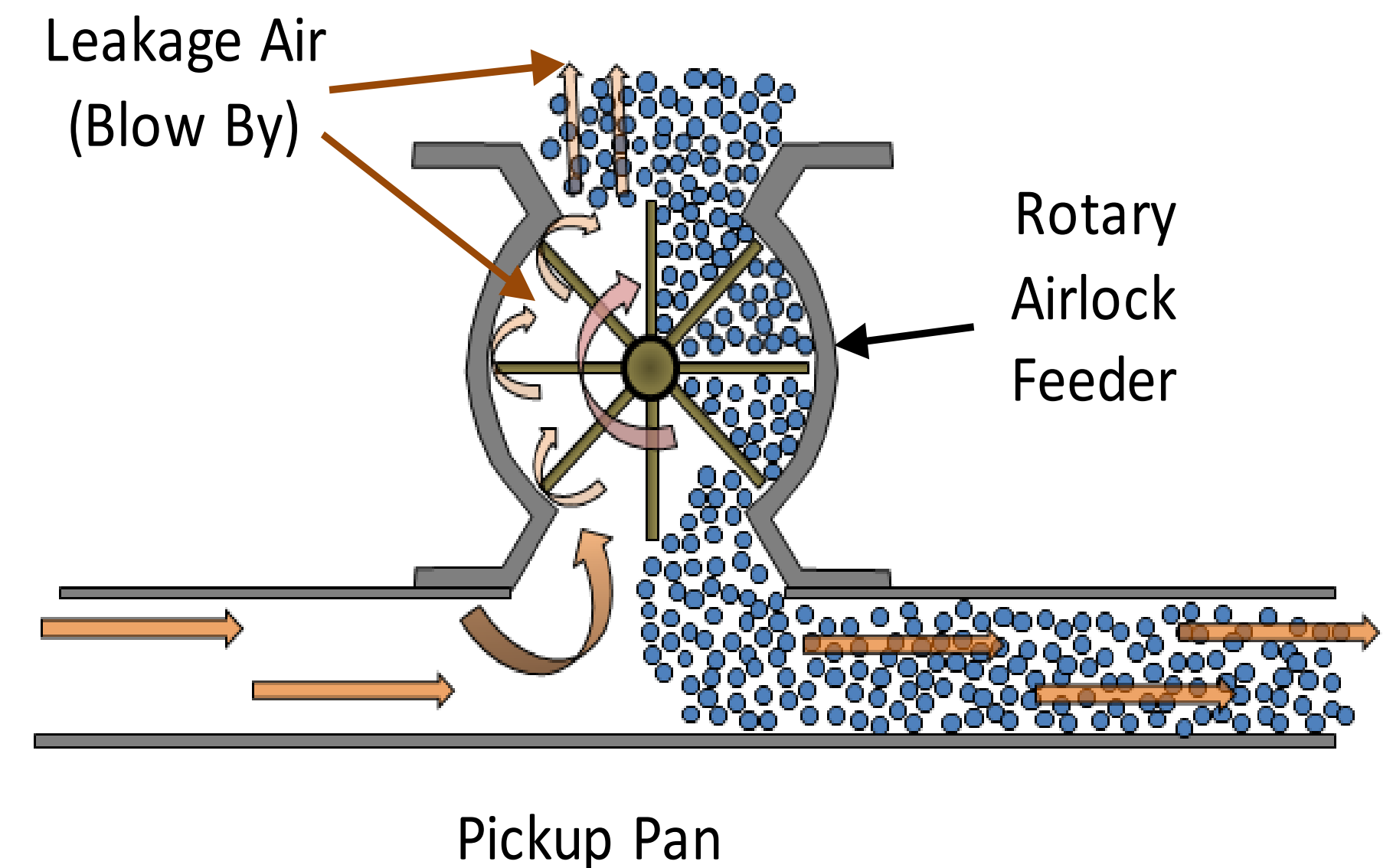
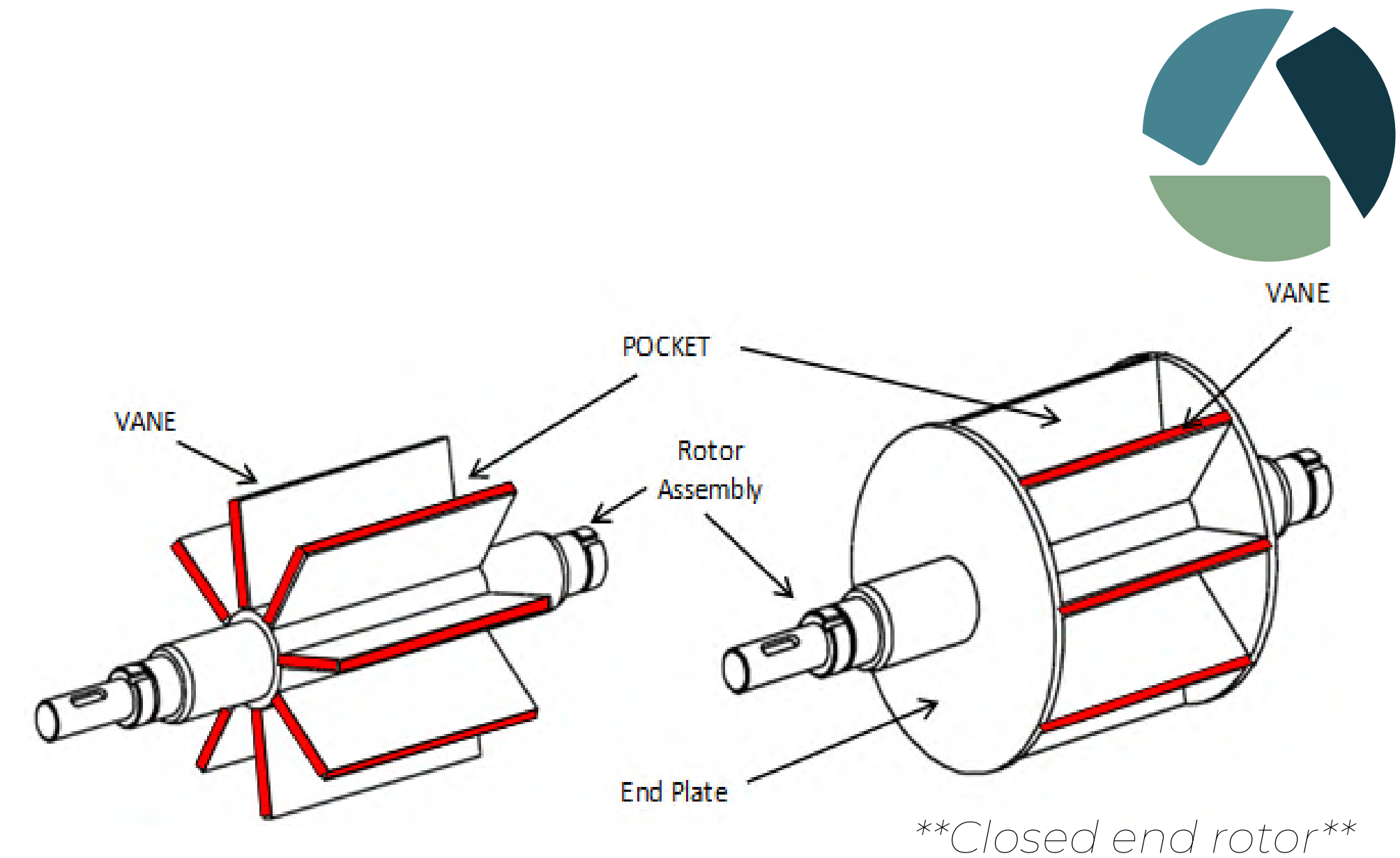
# Fluidization Key – Break Bridged Material

*Mass, not funnel flow*



# Rotary Feeders

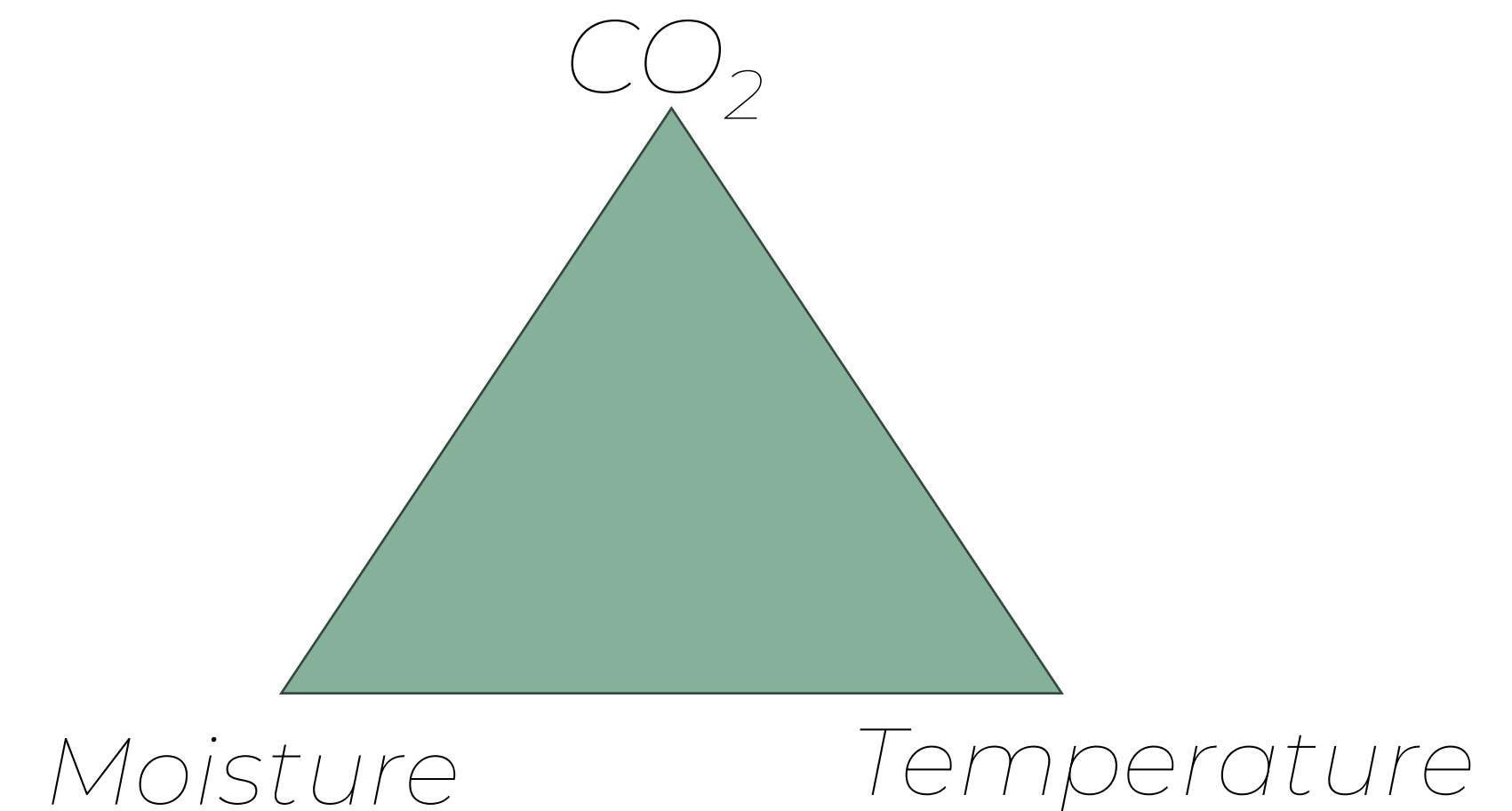
- Closed end rotors
- Consider shallow pocket valves to avoid slug flow
- Rotary Air Locks are wear items!
  - Abrasive and/or erosive effects
  - Reduction in conveying air velocity
  - Deposits in conveying line
  - Increase/Spikes in conveying air pressure
- Potential flooding with Screw Feeders
  - Rotary at inlet plus maintenance gate



# Conveying Issues – Deposit in Piping



- Hard Scale (calcium carbonate)
  - Short term formation – convey air effects
    - Quality
    - Quantity
  - Long term formation
    - Minimize physical ‘hot spots’
      - Unions and elbows
- Soft scale (hydrated lime powder)
  - Saltation velocity ~2,400 ft/min
  - Target 3,300-4,000 ft/min to keep hydrate suspended



***Scale formation is observed generally in Dry Sorbent Injection systems and usually not an issue in Circulating Dry Scrubbers***



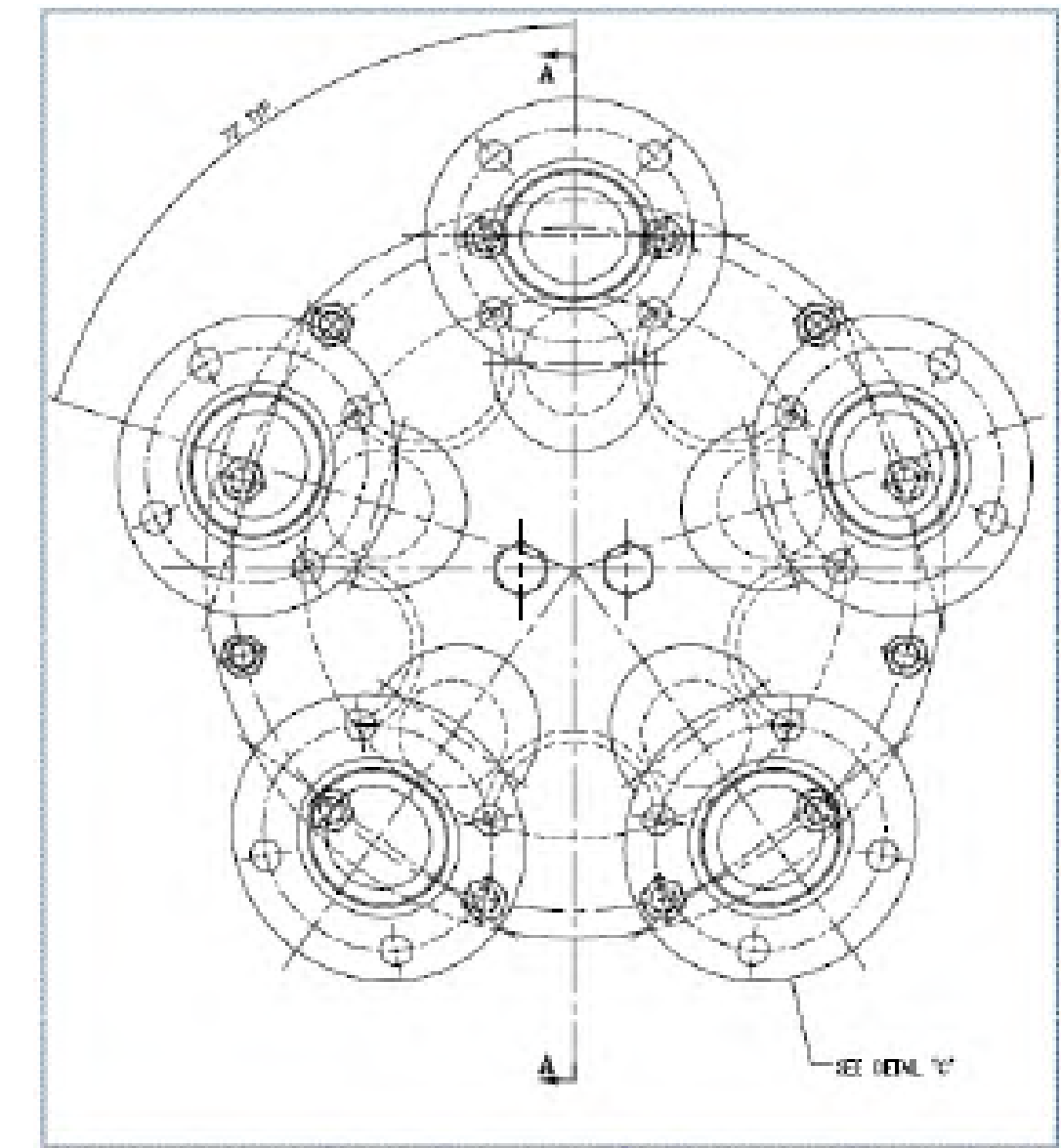
# Conveying Conditions at Hydrate Feed Point

- Limit moisture and extreme temperature in conveying air
- Convey air quantity
  - Above the pickup velocity (2,400 ft/min)
  - Below an amount that leads to scale buildup
  - Example on system with 4" ID pipe and operating at 5 psi

| Hydrate lb/hr | Blower SCFM | Pickup velocity | Hyd:Air | Comment                                                                |
|---------------|-------------|-----------------|---------|------------------------------------------------------------------------|
| 1500          | 300         | 2567 ft/min     | 1.03    | Low P/u velocity                                                       |
| 1500          | 400         | 3422 ft/min     | 0.77    | Good operating conditions                                              |
| 400           | 400         | 3422 ft/min     | 0.21    | Low Hyd:Air<br>Prone to scale buildup unless convey air is conditioned |
| 800           | 350         | 2994 ft/min     | 0.47    | Better than above but borderline                                       |

# Splitters

- Most successful DSI systems use a conical splitter
- Preference is upward split but descending splits can work
  - Horizontal is not recommended
  - Avoid elbows prior to a splitter
- Goal: equivalent flow to each leg
  - Equal lengths from splitter to lance
  - Resistive flow if equal lengths is not possible
- Consider troubleshooting and maintenance
  - Shut down a leg vs whole splitter
  - Avoid neckdowns in camlock fittings



# Post-splitter air flow

- Stay above saltation velocity between splitter and lances
- If below saltation, dry powder plugs form
  - No injection at that lance until plug is cleared

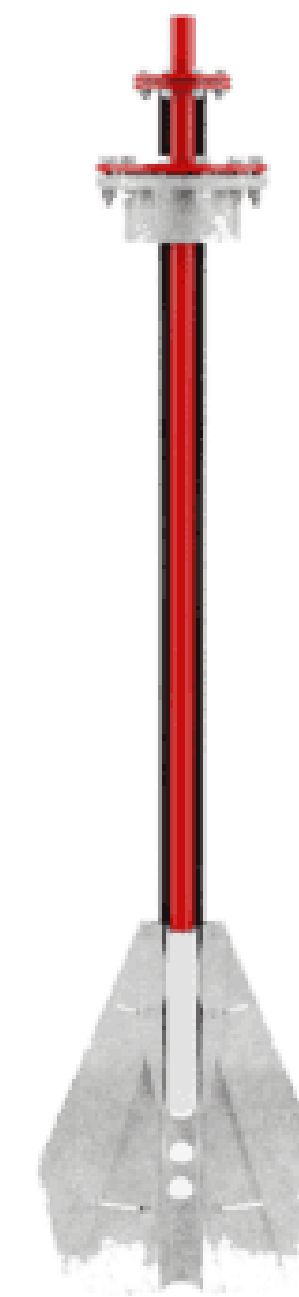
6 lances, 3 options on diameter

| Velocity, ft/min | Comment                               |
|------------------|---------------------------------------|
| < 2400           | Expect dry powder plugs               |
| 2400 – 3300      | suboptimal                            |
| >3300            | Good                                  |
| >5000            | Excess air; potential scale formation |

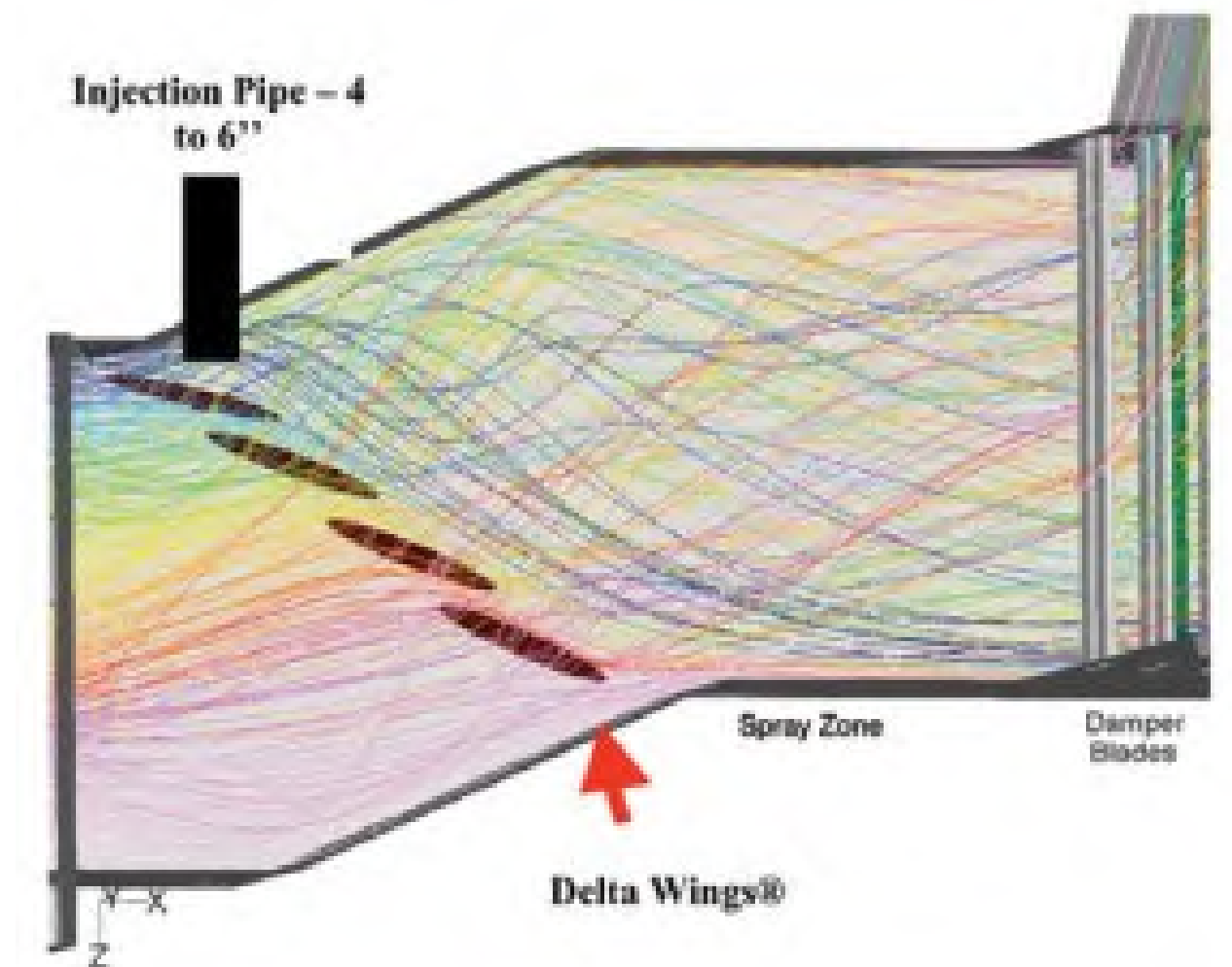
| Velocities In Line (Std Wall Sch 40) |                            |               |               |
|--------------------------------------|----------------------------|---------------|---------------|
| Pipe Size                            | 1.25                       | 1.5           | 2.0           |
| Pipe Dia. (I.D.)                     | 1.380                      | 1.610         | 2.067         |
| Sq Ft                                | <u>0.0104</u>              | <u>0.0141</u> | <u>0.0233</u> |
| # of Lines                           | 6                          | 6             | 6             |
| Total Sq Ft                          | <u>0.0623</u>              | <u>0.0848</u> | <u>0.1397</u> |
| 150                                  | 2,408                      | 1,769         | 1,073         |
| 170                                  | 2,729                      | 2,005         | 1,216         |
| 190                                  | 3,050                      | 2,241         | 1,360         |
| 210                                  | 3,371                      | 2,477         | 1,503         |
| 230                                  | 3,692                      | 2,713         | 1,646         |
| 250                                  | 4,014                      | 2,949         | 1,789         |
| 270                                  | 4,335                      | 3,185         | 1,932         |
| 290                                  | 4,656                      | 3,420         | 2,075         |
| 310                                  | 4,977                      | 3,656         | 2,218         |
| 330                                  | 5,298                      | 3,892         | 2,361         |
| 350                                  | 5,619                      | 4,128         | 2,505         |
| 370                                  | 5,940                      | 4,364         | 2,648         |
| 390                                  | 6,261                      | 4,600         | 2,791         |
| 410                                  | 6,582                      | 4,836         | 2,934         |
| 430                                  | 6,903                      | 5,072         | 3,077         |
| 450                                  | 7,224                      | 5,308         | 3,220         |
| Blower Output SCFM                   | Feet Per Minute Velocities |               |               |

# Injection Lances

- Early lances attempted to induce distribution
- Straight pipe less prone to Pluggage
  - No smaller than 1.25" diameter!
- Philosophies
  - “Just don’t plug”: pipe or shrouded lance
  - Improve coverage
    - Engineered fins on lance
    - Duct mounted engineered plates
    - Add more lances

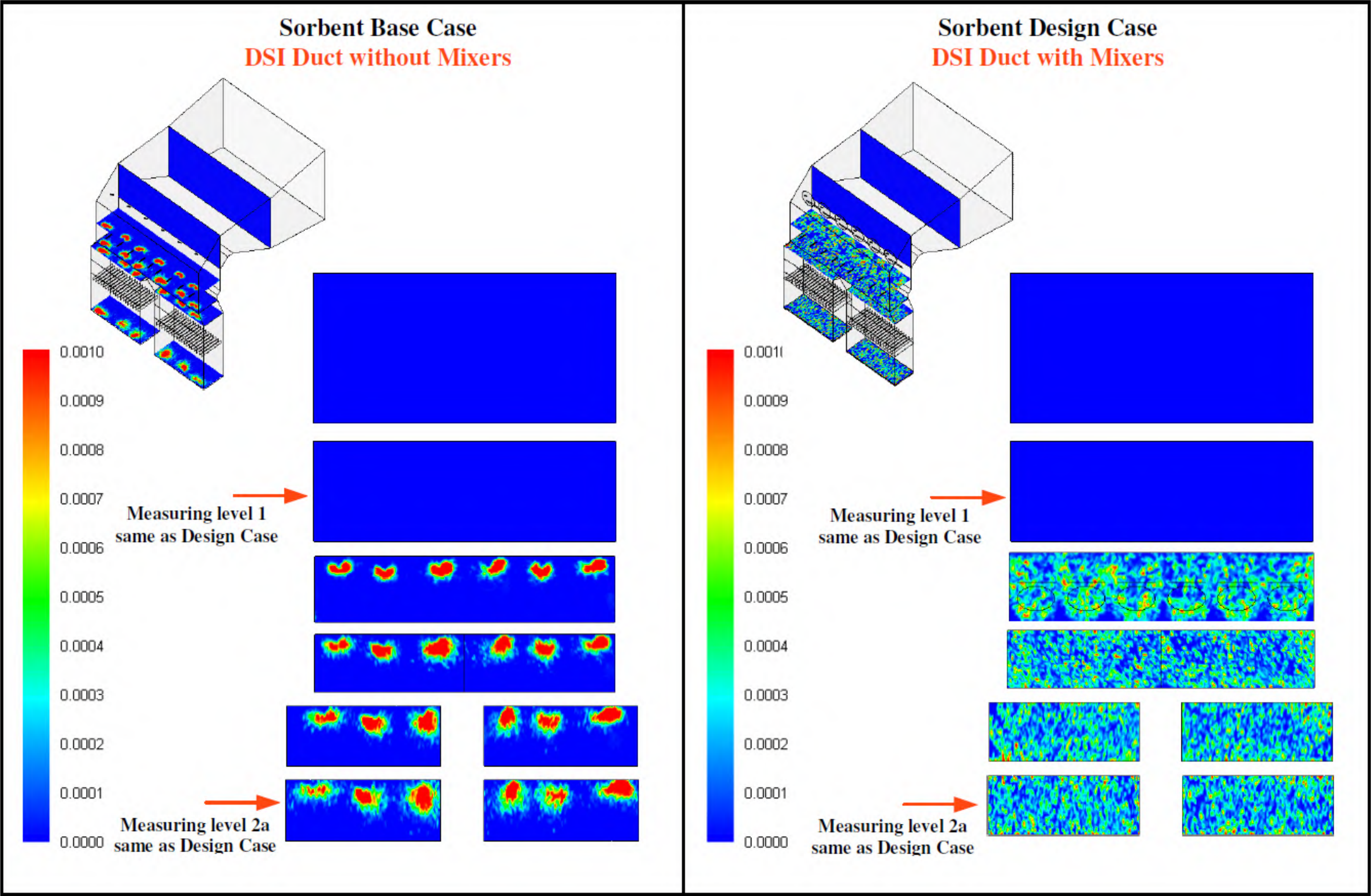


*UCC Cobra Lance*



*In Duct Mixing  
Babcock Power Delta Wings*

# Straight Pipe vs. Induced Distribution

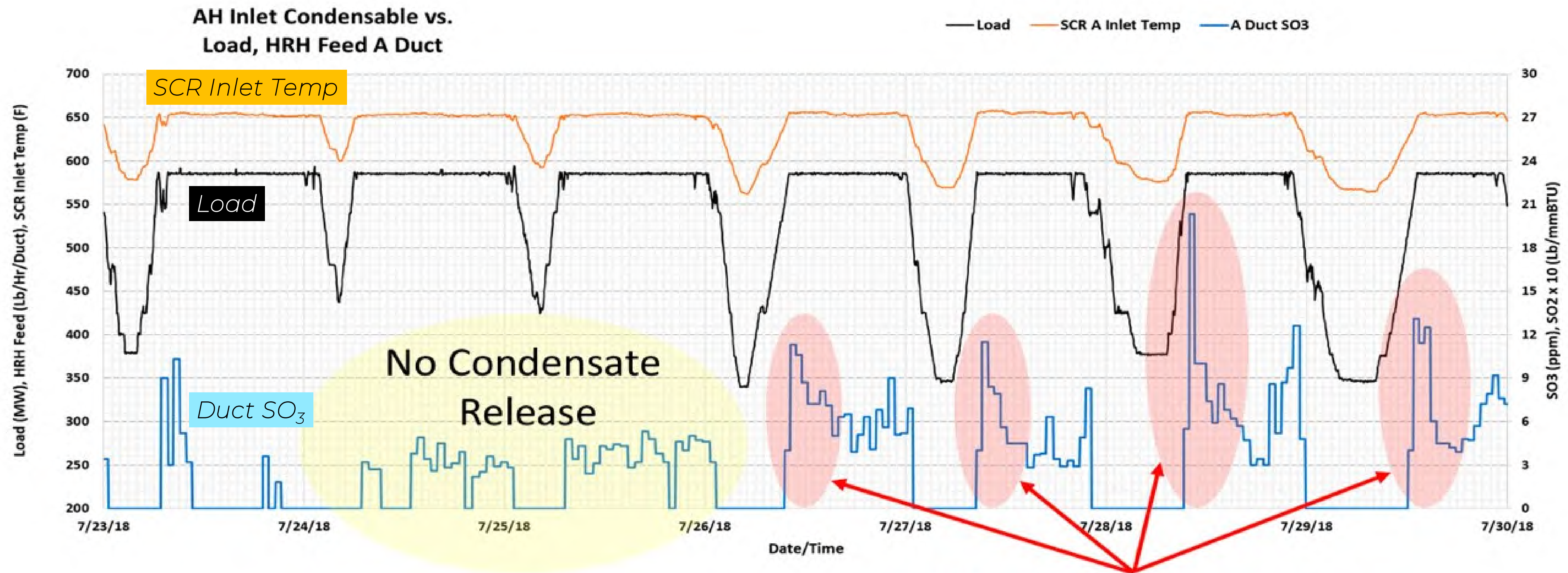


Provided by Babcock Power

# *Potential Pitfalls*



# Flue Gas Characteristics During Testing

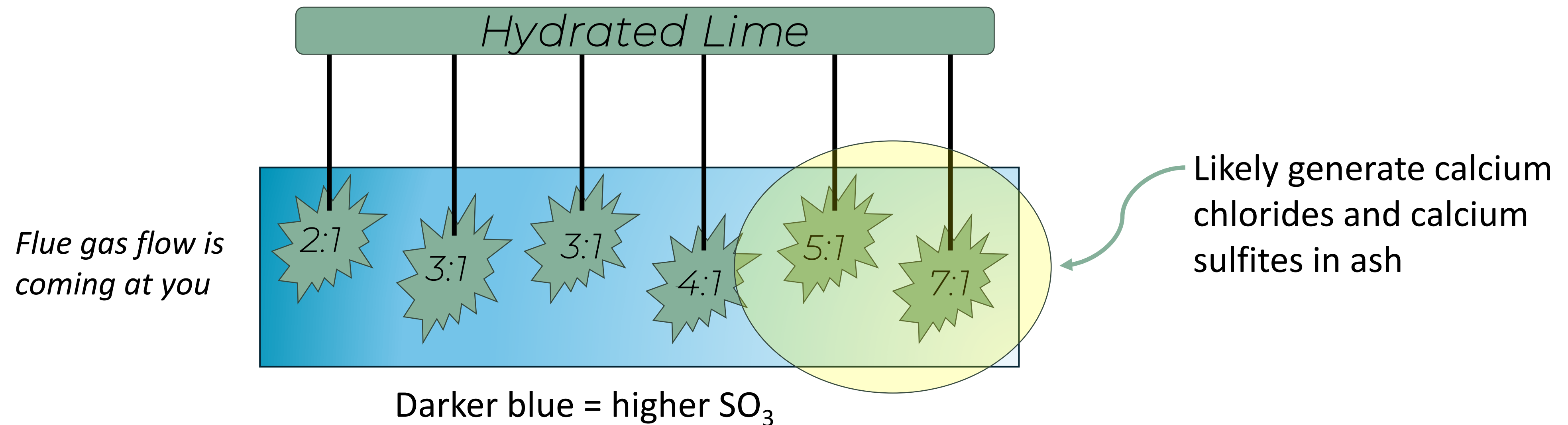


Not the same plant or test as previous slide

**Variable Condensate Release**

*Load ramp can cause condensable acid burn-off*  
*Make sure to account for this when stack testing*

# The Problem with Stratification



- Local NSR is different across the duct (Hydrate: $\text{SO}_3$ )
- Locally high levels of hydrate will react with any acid present to form the calcium salt ( $\text{HCl}$ ,  $\text{SO}_2$ , and  $\text{CO}_2$ )
- Stratification typically more problematic at post-APH injection locations

## *Other tips*



- Begin stack test with a full silo
- Evaluate high hydrate feed rate early for a quick litmus test
- Seasoning – it can be a thing
- Leave blowers running even if you shut down hydrate feed

*Thank you*



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*MLC*

*Booth 21*